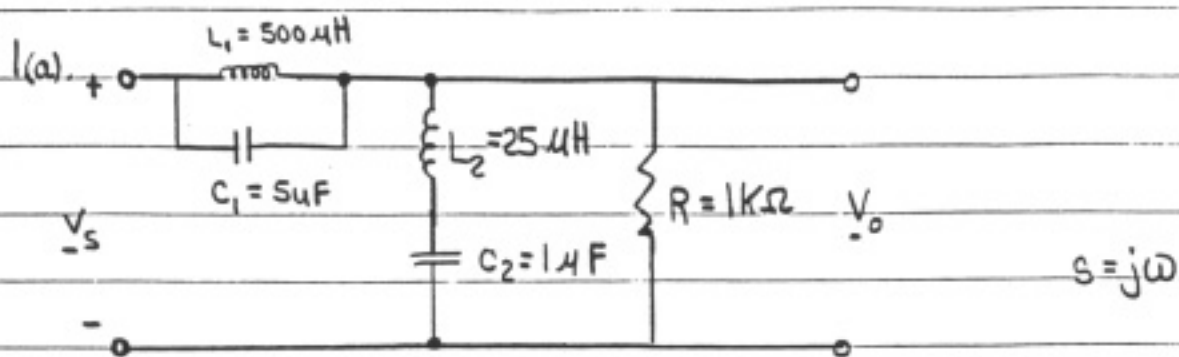


HW #12 Solutions

$$Z_{L_1 \parallel C_1} = \frac{sL_1 \left(\frac{1}{sC_1} \right)}{sL_1 + \frac{1}{sC_1}} = \frac{L_1 s}{1 + L_1 C_1 s^2}$$

$$Z_{L_2 + C_2} = \frac{1}{sC_2} + sL_2 = \frac{1 + L_2 C_2 s^2}{C_2 s}$$

$$Z_{(L_2 + C_2) \parallel R} = \frac{Z_{L_2 + C_2} \cdot R}{R + Z_{L_2 + C_2}} = \frac{R(1 + L_2 C_2 s^2)}{L_2 C_2 s^2 + R C_2 s + 1}$$

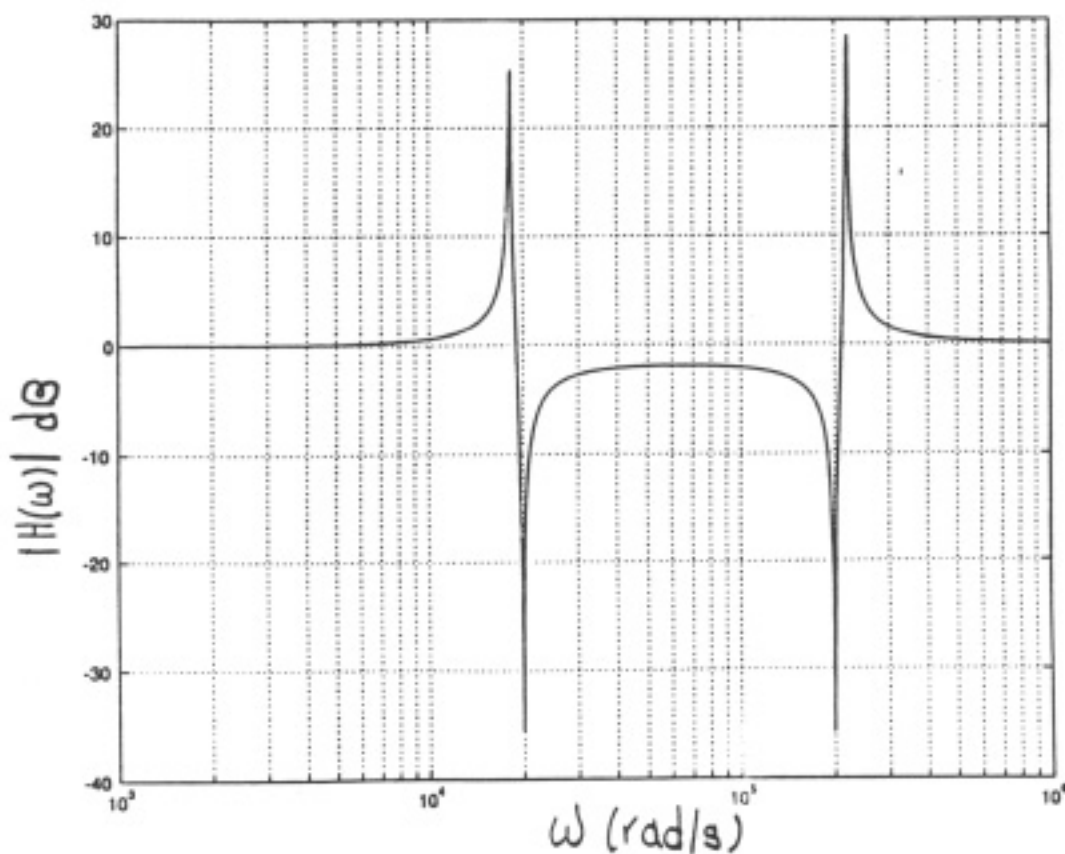
Voltage divider

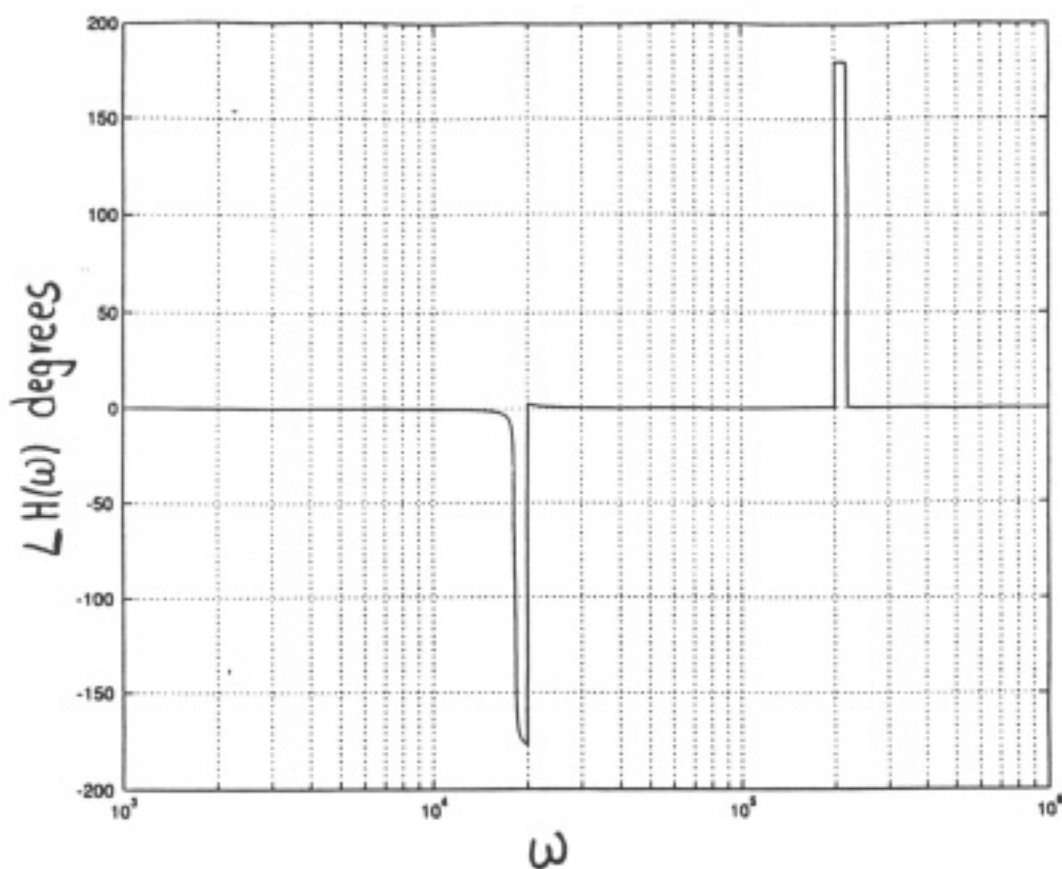
$$\begin{aligned}
 H(s) = \frac{V_o}{V_s} &= \frac{Z_{(L_2 + C_2) \parallel R}}{Z_{(L_2 + C_2) \parallel R} + Z_{L_1 \parallel C_1}} \\
 &= \frac{R(1 + L_2 C_2 s^2)(1 + L_1 C_1 s^2)}{R(1 + L_2 C_2 s^2)(1 + L_1 C_1 s^2) + L_1 s(L_2 C_2 s^2 + R C_2 s + 1)} \\
 &= \frac{R L_1 C_1 L_2 C_2 s^4 + R(L_1 C_1 + L_2 C_2) s^2 + R}{R L_1 C_1 L_2 C_2 s^4 + L_1 L_2 C_2 s^3 + [R(L_1 C_1 + L_2 C_2) + R L_1 C_2] s^2 + L_1 s + R}
 \end{aligned}$$

$$\therefore H(s) = \frac{6.25 \times 10^{-17} s^4 + 2.525 \times 10^{-6} s^2 + 10^3}{6.25 \times 10^{-17} s^4 + 1.25 \times 10^{-14} s^3 + 3.025 \times 10^{-6} s^2 + 5 \times 10^{-4} s + 10^3}$$

matlab program

```
(b) num = [6.25e-17 0 2.525e-6 0 1e3];
    denom = [6.25e-17 1.25e-14 3.025e-6 5e-4 1e3];
    W = logspace(3, 6, 1000);
    [mag, phase, W] = bode(num, denom, W);
    magdb = -20 * log10(mag);
    semilogx(W, mag);
    grid
    semilogx(W, phase);
    grid
```



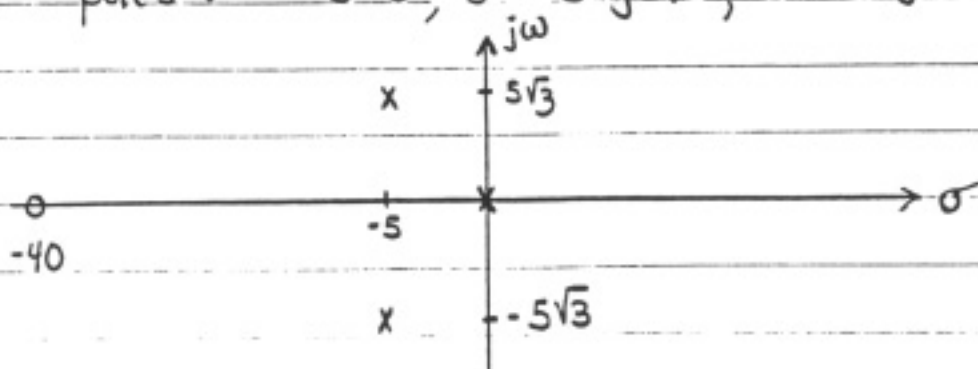


(c) Frequencies rejected are $2 \times 10^4 \text{ rad/s}$ & $2 \times 10^5 \text{ rad/s}$

2.
$$H(s) = \frac{10s + 400}{s^3 + 10s^2 + 100s}$$

Zeros : $s = -40$

poles : $s = 0$, $s = -5 - j5\sqrt{3}$, $s = -5 + j5\sqrt{3}$



HW #12 EECS 210 F99 Problem 2 (Bode plot solution)

$$H(s) = \frac{10s + 400}{s^3 + 10s^2 + 100s}$$

$$= 4 \frac{1 + s/40}{s[(s/10)^2 + s/10 + 1]}$$

$$= 4 \frac{1 + s/40}{s[(s/\omega_0)^2 + 2\zeta(s/\omega_0) + 1]}$$

where $\omega_0 = 10 \text{ rad/s}$ & $\zeta = .5$

4 terms

4

$s + 40$

s

asymptotic behavior

12 dB

0 dB over $0 \leq \omega \leq 40$ & slope +20 dB/decade over $\omega \geq 40$

0 dB @ $\omega = 1$ & slope -20 dB/decade

corner freq.

$$(s/\omega_0)^2 + 2\zeta(s/\omega_0) + 1$$

0 dB for $\omega \leq \omega_0$

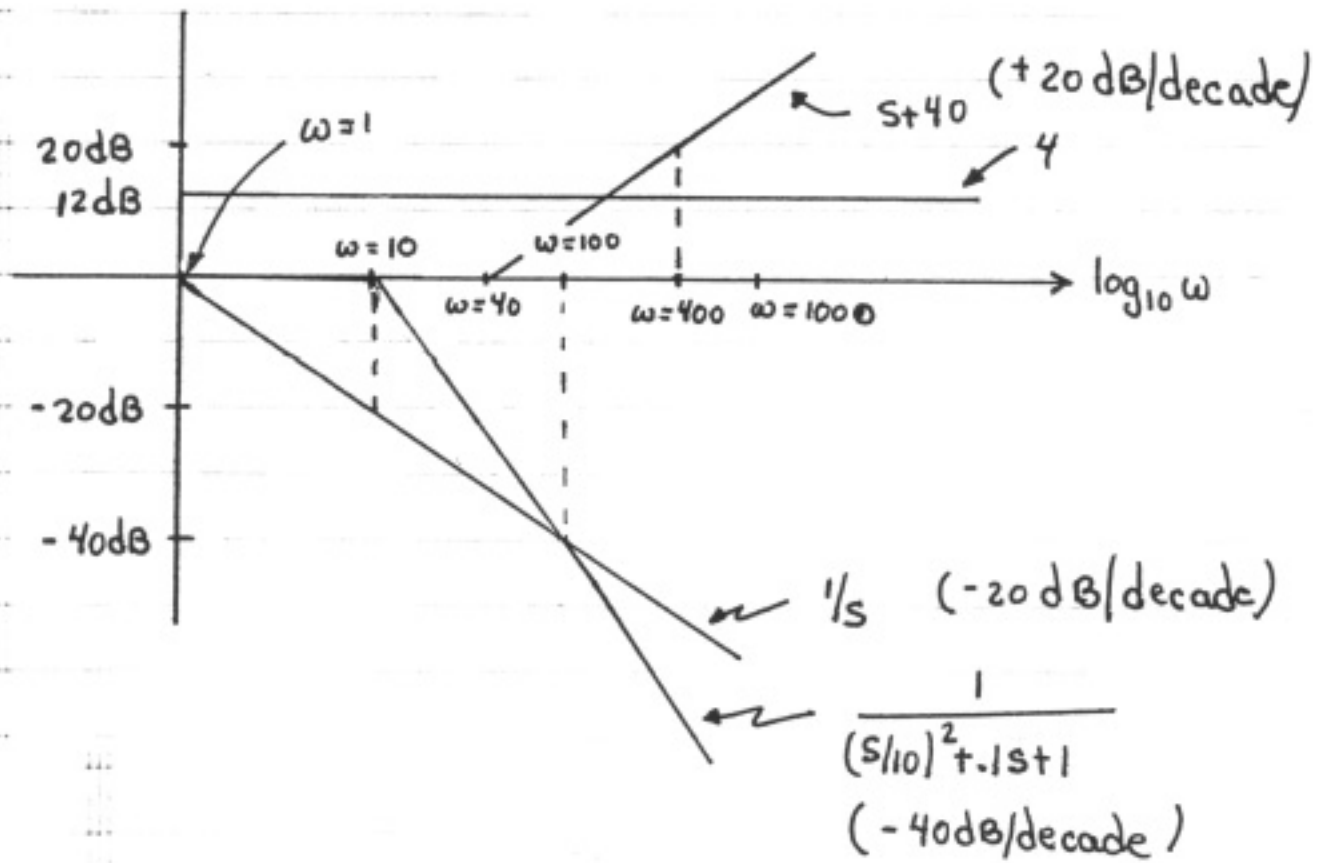
-40 dB/decade slope for $\omega > \omega_0$

More accurately

$$\omega_p = \omega_0 \sqrt{1 - 2\zeta^2} = .707\omega_0 = 7.07 \text{ rad/s}$$

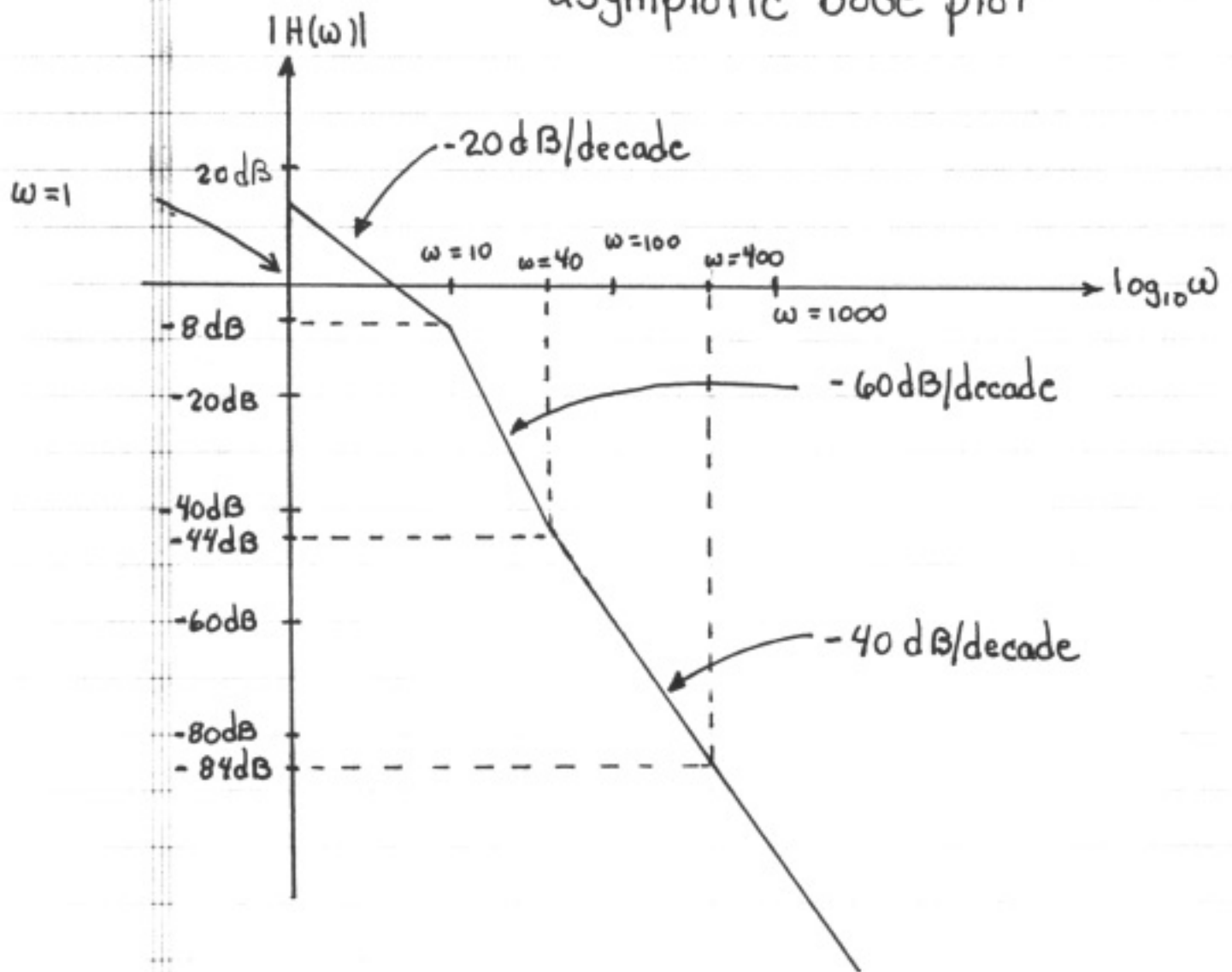
$$\max |H(\omega)| = \frac{1}{2\zeta[1 - \zeta^2]} = 1.33 \text{ (2.5 dB)}$$

freq. where max of $|H(\omega)|$ occurs



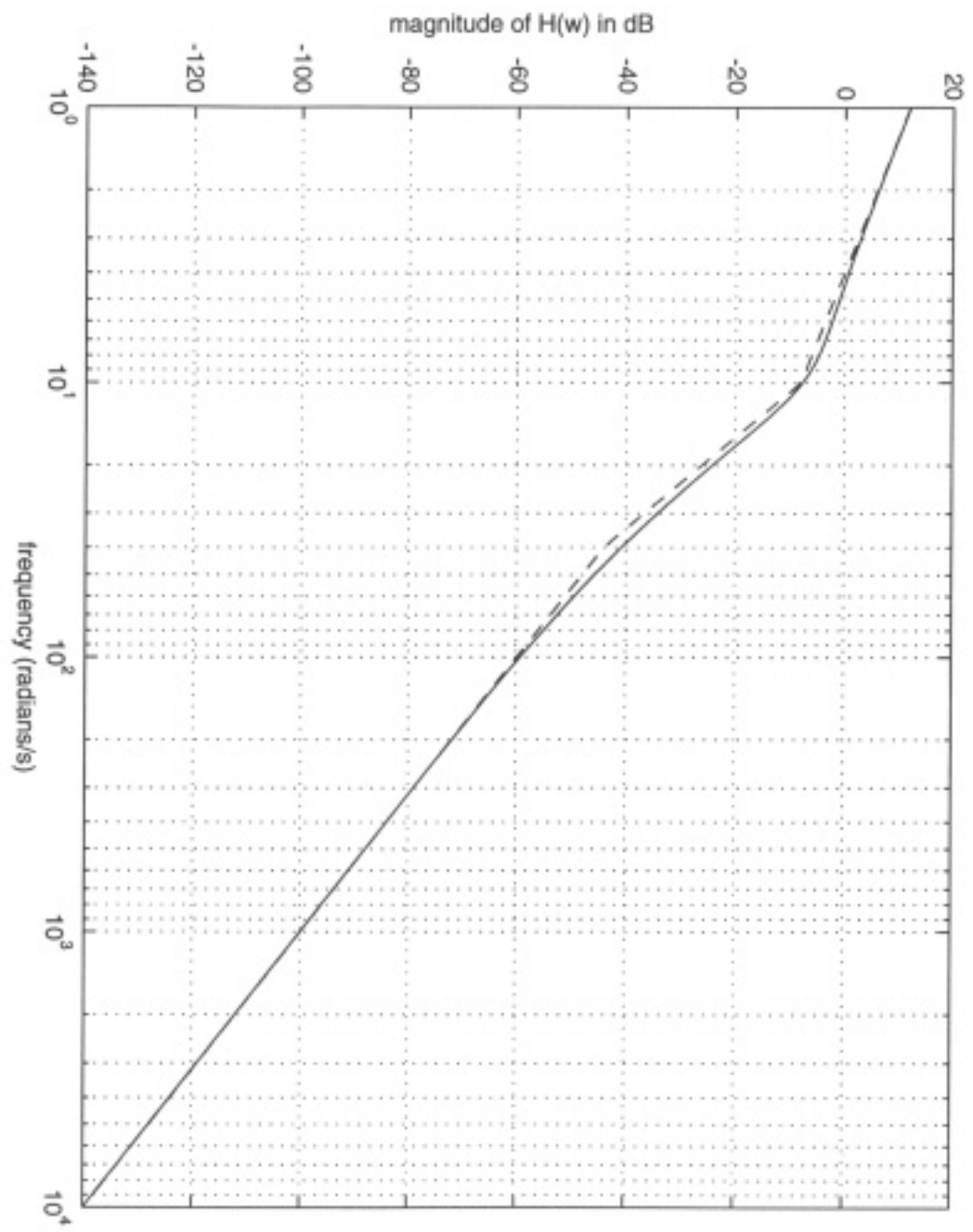
asymptotic bode plot

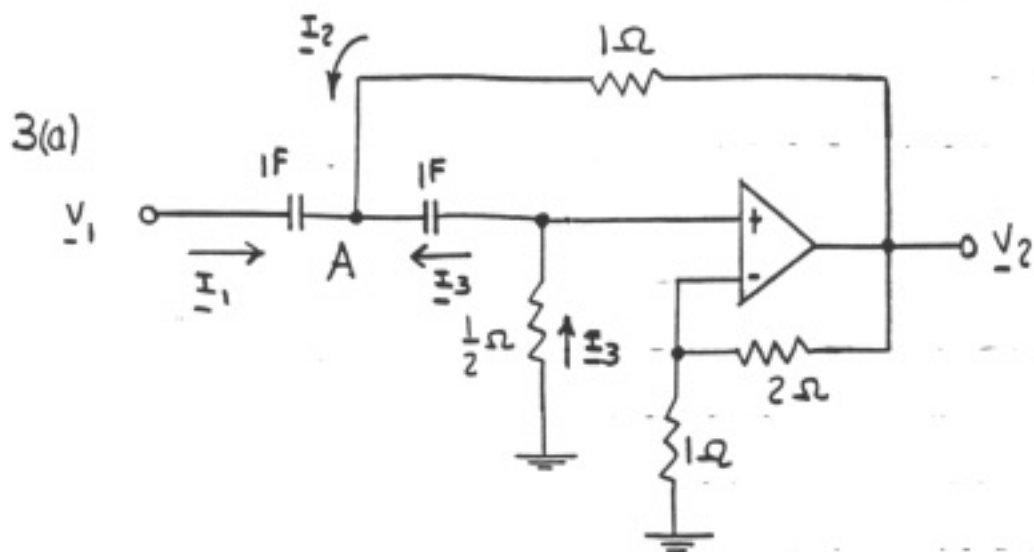
3



see next page for exact bode plot (solid curve) and asymptotic bode plot (--- curve) shown together

4





$$V_{(-)} = V_2 / 3 \quad (1) \quad (\text{voltage divider})$$

$$V_{(+)} = V_{(-)} = V_2 / 3 \quad (2)$$

$$\therefore I_3 = \frac{0 - V_{(+)}}{1/2} = -\frac{2}{3} V_2 \quad (3)$$

$$V_A = V_{(+)} - I_3 Z_{1F} \quad (4)$$

$$= \frac{V_2}{3} + \frac{2}{3} V_2 \frac{1}{j\omega} \quad (5)$$

$$I_2 = \frac{V_2 - V_A}{1\Omega} = \frac{2}{3} V_2 - \frac{2}{3} V_2 \frac{1}{j\omega} \quad (6)$$

$$I_1 + I_2 + I_3 = 0 \quad (7)$$

$$\therefore I_1 = -\frac{2}{3} V_2 + \frac{2}{3} V_2 \frac{1}{j\omega} + \frac{2}{3} V_2 = \frac{2}{3} V_2 \frac{1}{j\omega} \quad (8)$$

$$V_1 - V_A = I_1 Z_{1F} \quad (9)$$

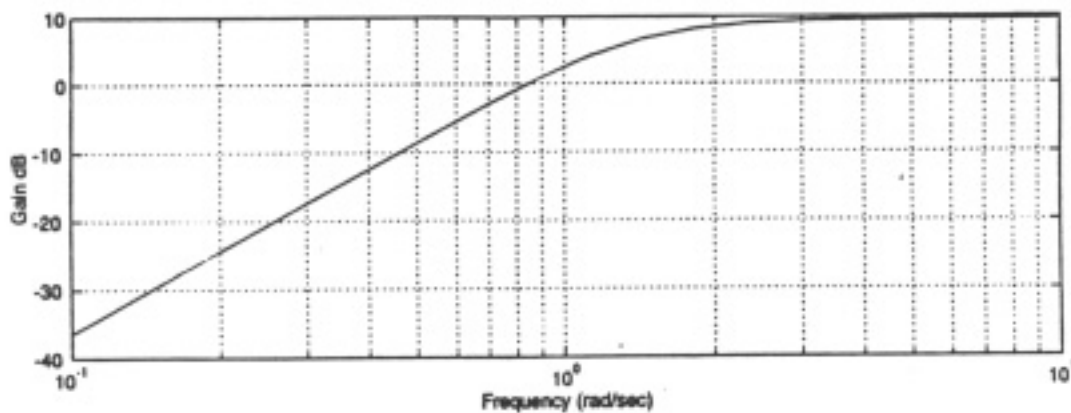
$$= \frac{2}{3} V_2 \frac{1}{j\omega} \frac{1}{j\omega} = -\frac{2}{3\omega^2} V_2 \quad (10)$$

$$\therefore V_1 = \frac{V_2}{3} + \frac{2}{3} V_2 \frac{1}{j\omega} - \frac{2}{3\omega^2} V_2 \quad (11)$$

$$\therefore H(\omega) = \frac{3}{1 + \frac{2}{j\omega} + \frac{2}{(j\omega)^2}} \quad (12)$$

$$H(s) = \frac{3s^2}{s^2 + 2s + 2} \quad (13)$$

A second order high pass filter.



from Eq. (13)

$$(b) |H(\omega = \infty)| = 3 \quad (14)$$

$$|H(\omega_c)| = .707 |H(\omega = \infty)| \quad (15)$$

$$|H(\omega_c)| = \frac{3\omega_c^2}{\sqrt{(2 - \omega_c^2)^2 + 4\omega_c^2}} = \frac{3\omega_c^2}{\sqrt{4 + \omega_c^4}} \quad (16)$$

Combining Eqs. (14)-(16) yields

$$.707 = \frac{\omega_c^2}{\sqrt{4 + \omega_c^4}}$$

$$\Rightarrow \omega_c = \sqrt{2} \text{ rad/s}$$

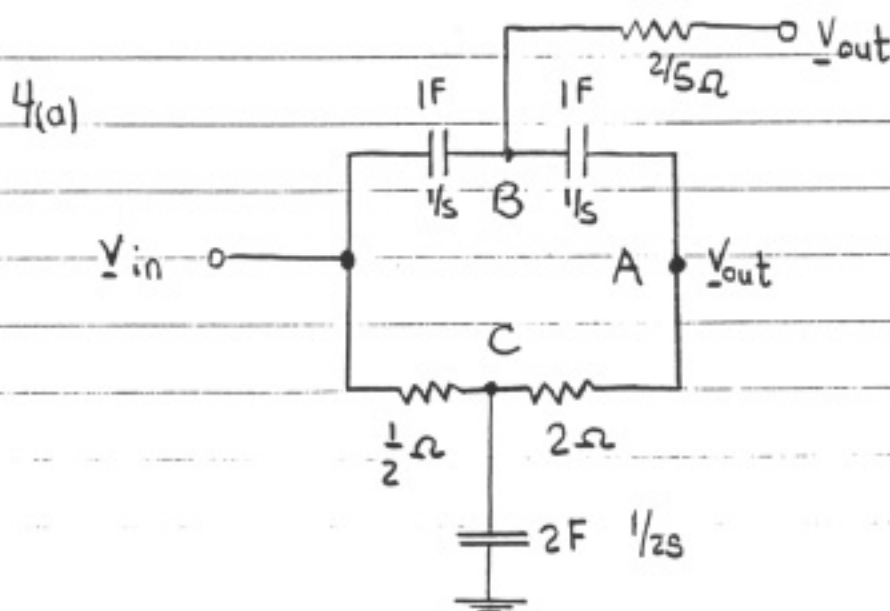
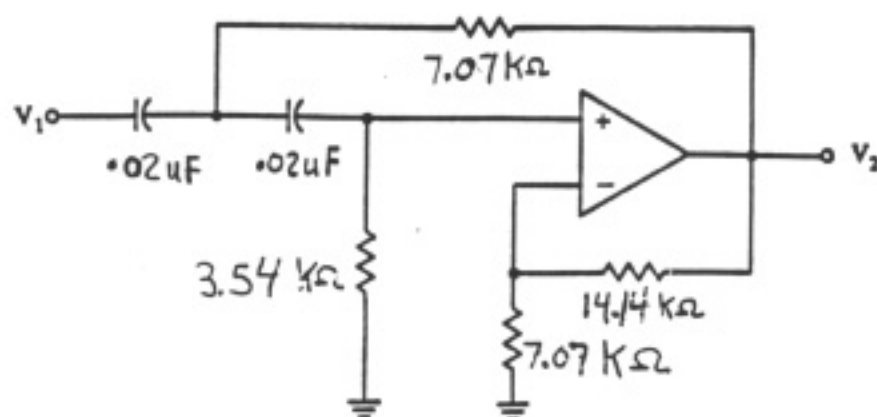
$$k_f = \frac{10^4}{\omega_c} = 7.072 \times 10^3$$

$$C_{\text{new}} = 0.02 \times 10^{-6} = \frac{C_{\text{old}}}{k_m k_f} = \frac{1}{7.07 \times 10^3 k_m}$$

$$\therefore k_m = 7.07 \times 10^3$$

$$R_{\text{new}} = k_m R_{\text{old}} = 7.07 \times 10^3 R_{\text{old}}$$

Thus the scaled circuit becomes



Write node equations @ nodes A, B & C.

$$@ A : (V_B - V_{out})s + (V_C - V_{out})\frac{1}{2} = 0 \quad (1)$$

$$\therefore (s + \frac{1}{2})V_{out} - sV_B - \frac{1}{2}V_C = 0 \quad (2)$$

$$@ B : (V_{in} - V_B)s + (V_{out} - V_B)\frac{5}{2} + (V_{out} - V_B)s = 0 \quad (3)$$

$$\therefore (2s + \frac{5}{2})V_B - (s + \frac{5}{2})V_{out} = sV_{in} \quad (4)$$

$$@ C : (V_{in} - V_C)2 + (0 - V_C)2s + (V_{out} - V_C) \cdot 5 = 0 \quad (5)$$

$$\therefore (2s + \frac{5}{2})V_C - \frac{1}{2}V_{out} = 2V_{in} \quad (6)$$

From (4)

$$V_B = \frac{(2s+5)V_{out} + 2sV_{in}}{4s+5} \quad (7)$$

From (6)

$$V_C = \frac{V_{out} + 4V_{in}}{4s+5} \quad (8)$$

Substituting Eqs. (7) & (8) into Eq. (1) yields

$$H(s) = \frac{V_{out}}{V_{in}} = \frac{s^2 + 1}{s^2 + s + 1} \quad (9)$$

See Eq. (9.25) in your notes for a bandstop filter

$$H(s) = \frac{s^2 + \omega_0^2}{s^2 + (\Delta\omega)s + \omega_0^2} \quad (10)$$

Comparing Eqs. (9) & (10) we see that

$$\omega_0 = 1 \text{ rad/s}$$

$$\Delta\omega = 1 \text{ rad/s}$$

$$\Rightarrow Q = \frac{\omega_0}{\Delta\omega} = 1$$

$$(b) \quad K_f = \frac{2\pi \times 60}{\omega_0} = \frac{2\pi \times 60}{1} = 377$$

$$1 \text{ nF} = C_{\text{new}} = \frac{C_{\text{old}}}{K_m K_f} = \frac{1 \text{ F}}{K_f K_m} = \frac{1 \text{ F}}{377 K_m}$$

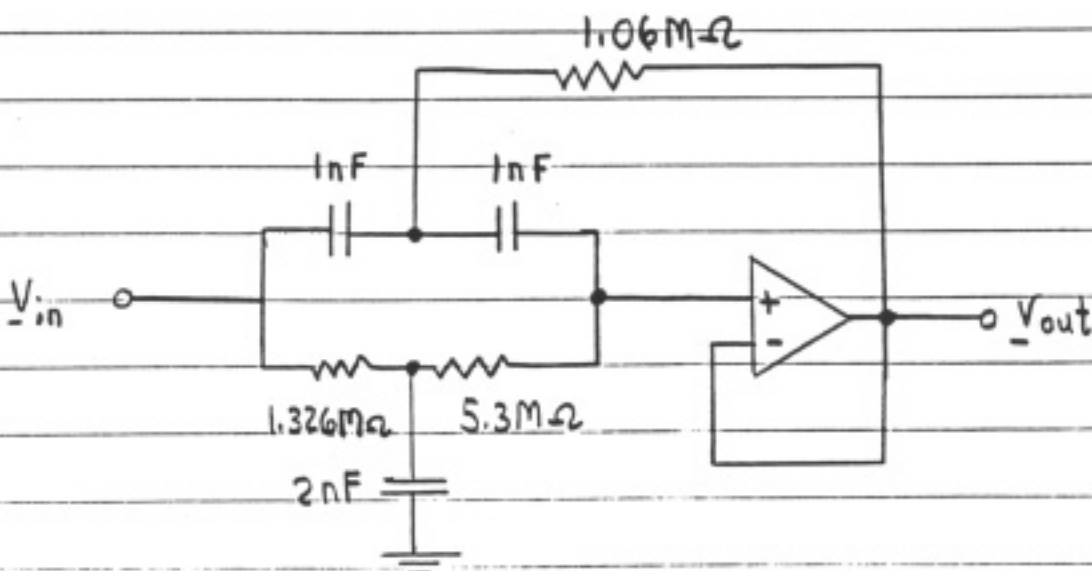
$$\Rightarrow K_m = 2.652 \times 10^6$$

$$\therefore R_{\text{new}} = K_m R_{\text{old}} = 2.652 \times 10^6 R_{\text{old}}$$

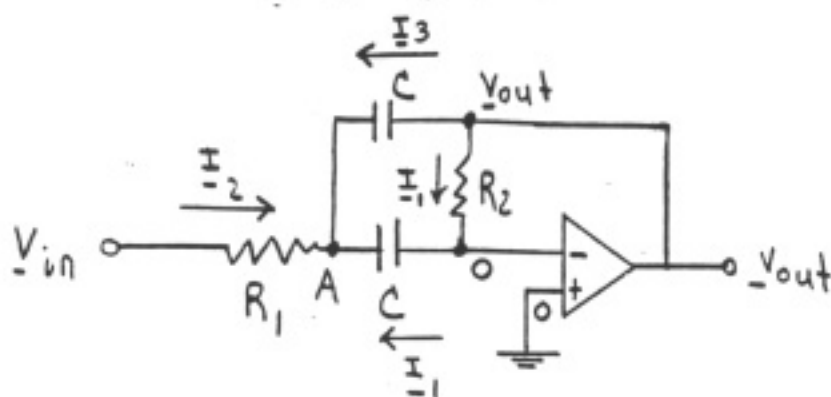
$$\Rightarrow \frac{1}{2} \Omega \rightarrow 1.326 \text{ M}\Omega$$

$$2 \Omega \rightarrow 5.3 \text{ M}\Omega$$

$$\frac{2}{5} \Omega \rightarrow 1.06 \text{ M}\Omega$$



5 (a) similar to Op Amp problem on exam #2



$$I_1 = V_{out} / R_2 \quad (1)$$

$$\therefore V_A = -I_1 \frac{1}{sC} = -\frac{V_{out}}{R_2 sC} \quad (2)$$

$$I_3 = (V_{out} - V_A) sC = V_{out} \left[1 + \frac{1}{R_2 sC} \right] sC \quad (3)$$

$$I_2 = -I_1 - I_3 = -V_{out} \left[\frac{2}{R_2} + sC \right] \quad (4)$$

$$V_{in} - V_A = I_2 R_1 \quad (5)$$

$$\therefore V_{in} = \frac{-V_{out}}{R_2 sC} - V_{out} \left[\frac{2R_1}{R_2} + sR_1 C \right] \quad (6)$$

$$\Rightarrow \boxed{H(s) = \frac{V_{out}}{V_{in}} = \frac{-R_2 sC}{R_1 R_2 C^2 s^2 + 2R_1 sC + 1}} \quad (7)$$

(b) Recall from Eq. (9.24) in your notes that

$$H(s) = \frac{(\Delta\omega)s}{s^2 + (\Delta\omega)st\omega_0^2} \quad (8)$$

is a bandpass filter. Comparing Eqs. (7) & (8) yields

$$\omega_0 = \frac{1}{\sqrt{R_1 R_2} C}$$

center freq. (9)

$$\Delta\omega = \frac{2}{R_2 C}$$

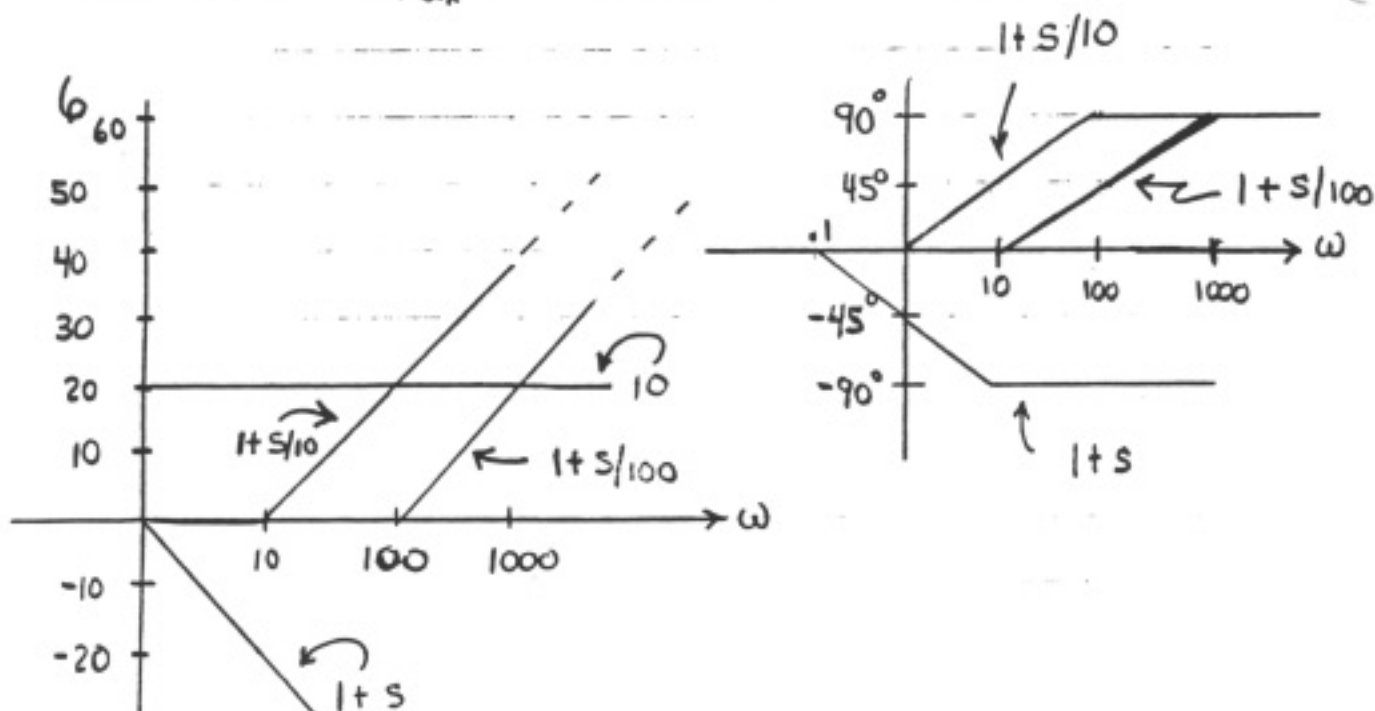
FWHM bandwidth (10)

(c) $\omega_0 = 2\pi \times 500 = \frac{1}{\sqrt{R_1 R_2} 10^{-8}}$

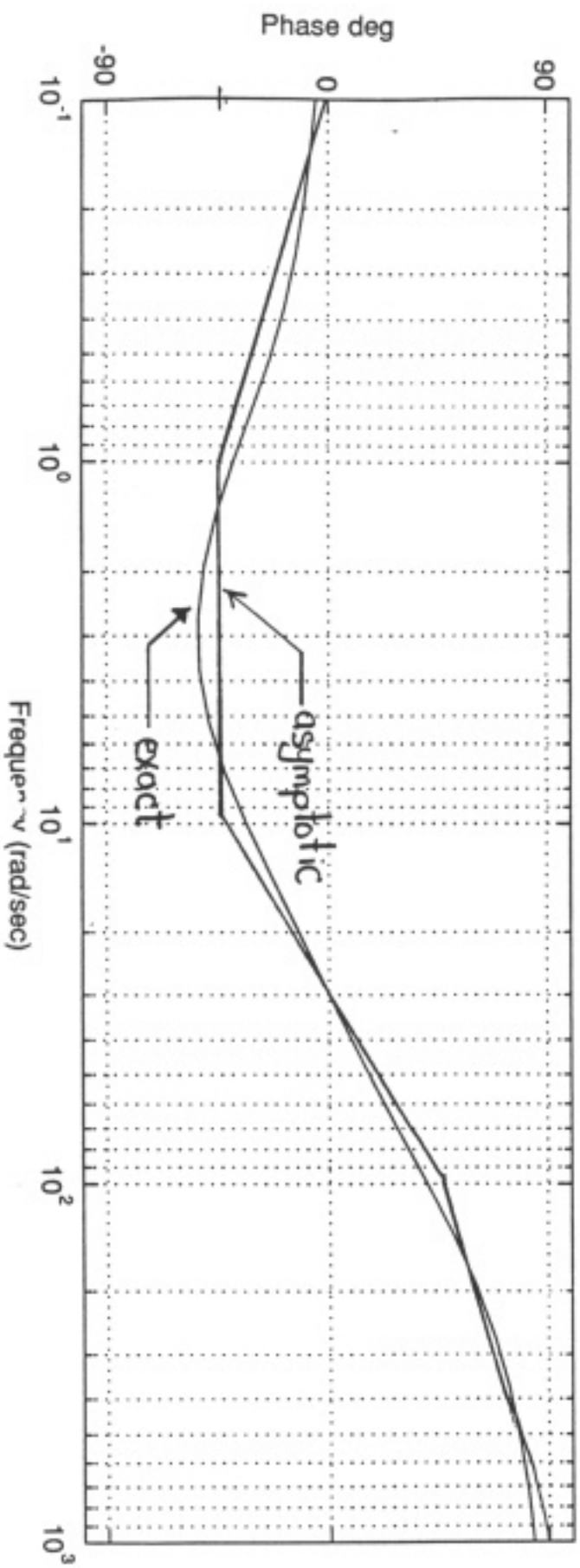
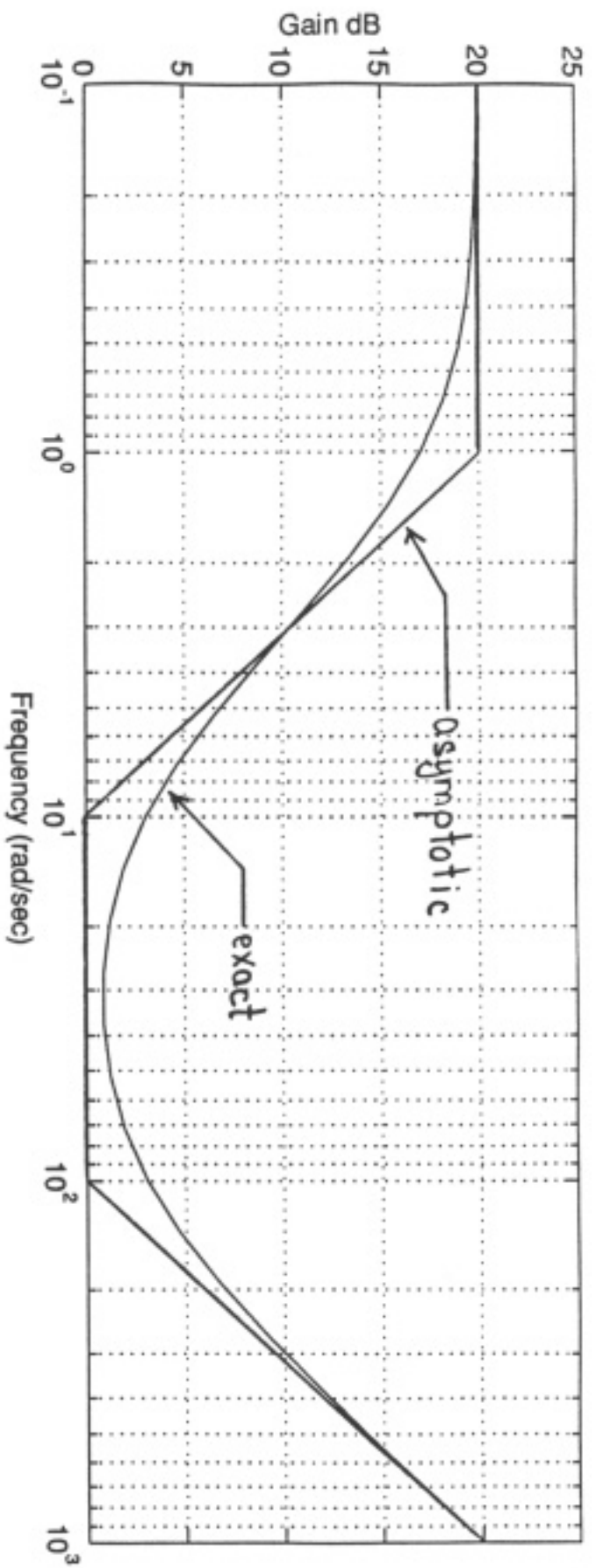
$$\Delta\omega = 2\pi \times 50 = \frac{2}{R_2 10^{-8}}$$

$$\therefore \underline{R_2 = 636.6 \text{ k}\Omega} \text{ \& } \underline{R_1 = 1.59 \text{ k}\Omega}$$

Also note $|H|_{\max} = R_2 / (2R_1) = 46 \text{ dB}$



(see next page)



7.

$$H(s) \approx .02 \frac{(1+s/.1)^2}{(1+s/.7)^2} \frac{(1+s/10)}{(1+s/100)} \frac{1}{(1+s/600)^2}$$

Because:

$$.02 \rightarrow -34 \text{ dB}$$

$$(1+s/.1)^2 \quad +40 \text{ dB/decade with corner freq. } \omega = .1 \text{ rad/s}$$

$$(1+s/.7)^2 \quad -40 \text{ dB/decade with corner freq. } \omega = .7 \text{ rad/s}$$

$$(1+s/10) \quad +20 \text{ dB/decade with corner freq. } \omega = 10 \text{ rad/s}$$

$$(1+s/100) \quad -20 \text{ dB/decade with corner freq. } \omega = 100 \text{ rad/s}$$

$$(1+s/600)^2 \quad -40 \text{ dB/decade with corner freq. } \omega = 600 \text{ rad/s}$$