

**University of Michigan**  
**EECS 311: Electronic Circuits**  
**Fall 2008**

Quiz 2

11/3/2008

NAME: Solutions

**Honor Code:**

I have neither given nor received unauthorized aid on this examination, nor have I concealed any violations of the Honor Code.

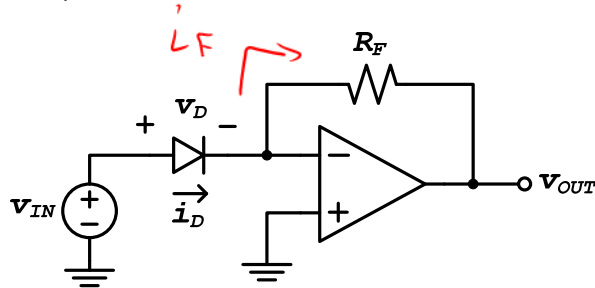
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Problem	Points	Score	Initials
1	26		
2	20		
3	30		
4	24		
	Total		



**Problem 1 (26 Points):** Potpourri – this problem has four unrelated parts.

- a) Find the expression for gain  $A_v = v_{OUT}/v_{IN}$  of the circuit below. Use the exact model for the diode,  $i_D = I_S(e^{v_D/V_T} - 1)$ . Assume the opamp is ideal.



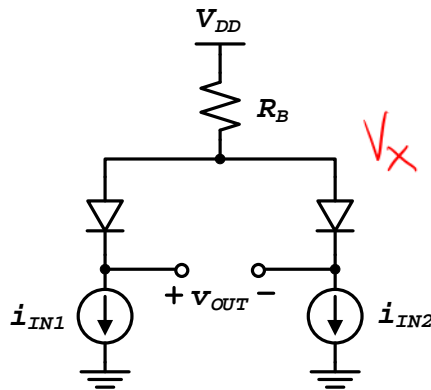
Cannot solve for  $\frac{v_{OUT}}{v_{IN}}$  !

$$i_F = i_D = I_S (e^{v_{IN}/V_T} - 1)$$

$$v_{OUT} = -R_F I_S (e^{v_{IN}/V_T} - 1)$$

Accepted all answers showing the above relationship between  $v_{OUT}$  and  $v_{IN}$

- b) Find an expression for the voltage  $v_{OUT}$  for the circuit below assuming  $i_{IN1} > 0$  and  $i_{IN2} > 0$ . Use the exact model for the diodes,  $i_D = I_S(e^{v_D/V_T} - 1)$ , assuming the two diodes are identical (same values for  $I_S$  and same temperature).



$$V_X = V_{DD} - R_B (i_{IN1} + i_{IN2})$$

$$v_{OUT} = (V_X - V_{D1}) - (V_X - V_{D2})$$

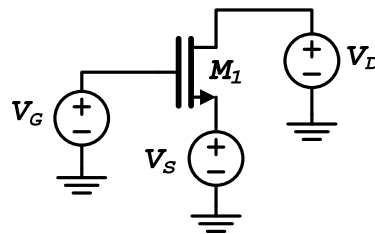
$$= V_{D2} - V_{D1}$$

$$V_{D2} = V_T \ln \left( \frac{i_{IN2}}{I_S} + 1 \right)$$

$$V_{D1} = V_T \ln \left( \frac{i_{IN1}}{I_S} + 1 \right)$$

$$v_{OUT} = V_T \ln \left[ \frac{\frac{i_{IN2}}{I_S} + 1}{\frac{i_{IN1}}{I_S} + 1} \right]$$

- c) Identify the region of operation of  $M_1$  in the circuit below when  $V_G = 2\text{ V}$ ,  $V_D = 3\text{ V}$ , and  $V_S = -1\text{ V}$ . Assume  $V_{TN} = 1\text{ V}$  and ignore the body-effect on threshold voltage.



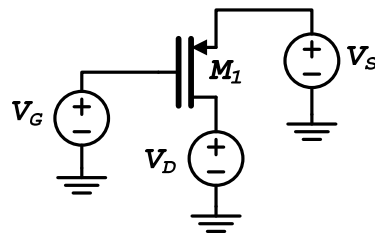
$$V_{GS} = 2 - (-1) = 3\text{ V}$$

$$V_{GS} > V_{TN} \Rightarrow \text{ON}$$

$$V_{DS} = 3 - (-1) = 4\text{ V}$$

$$V_{DS} > V_{GS} - V_{TN} \Rightarrow \boxed{\text{SAT}}$$

- d) Identify the region of operation of  $M_1$  in the circuit below when  $V_G = 3\text{ V}$ ,  $V_D = 5\text{ V}$ , and  $V_S = 5\text{ V}$ . Assume  $V_{TP} = -1\text{ V}$  and ignore the body-effect on threshold voltage.



$$V_{GS} = 3 - 5 = -2\text{ V}$$

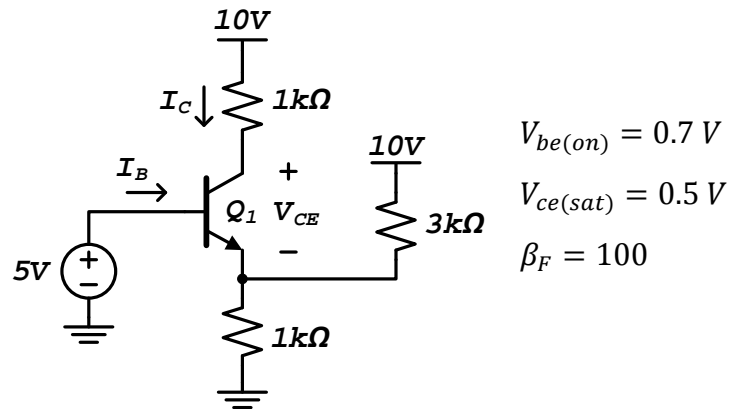
$$|V_{GS}| > |V_{TP}| \Rightarrow \text{ON}$$

$$V_{DS} = 5 - 5 = 0$$

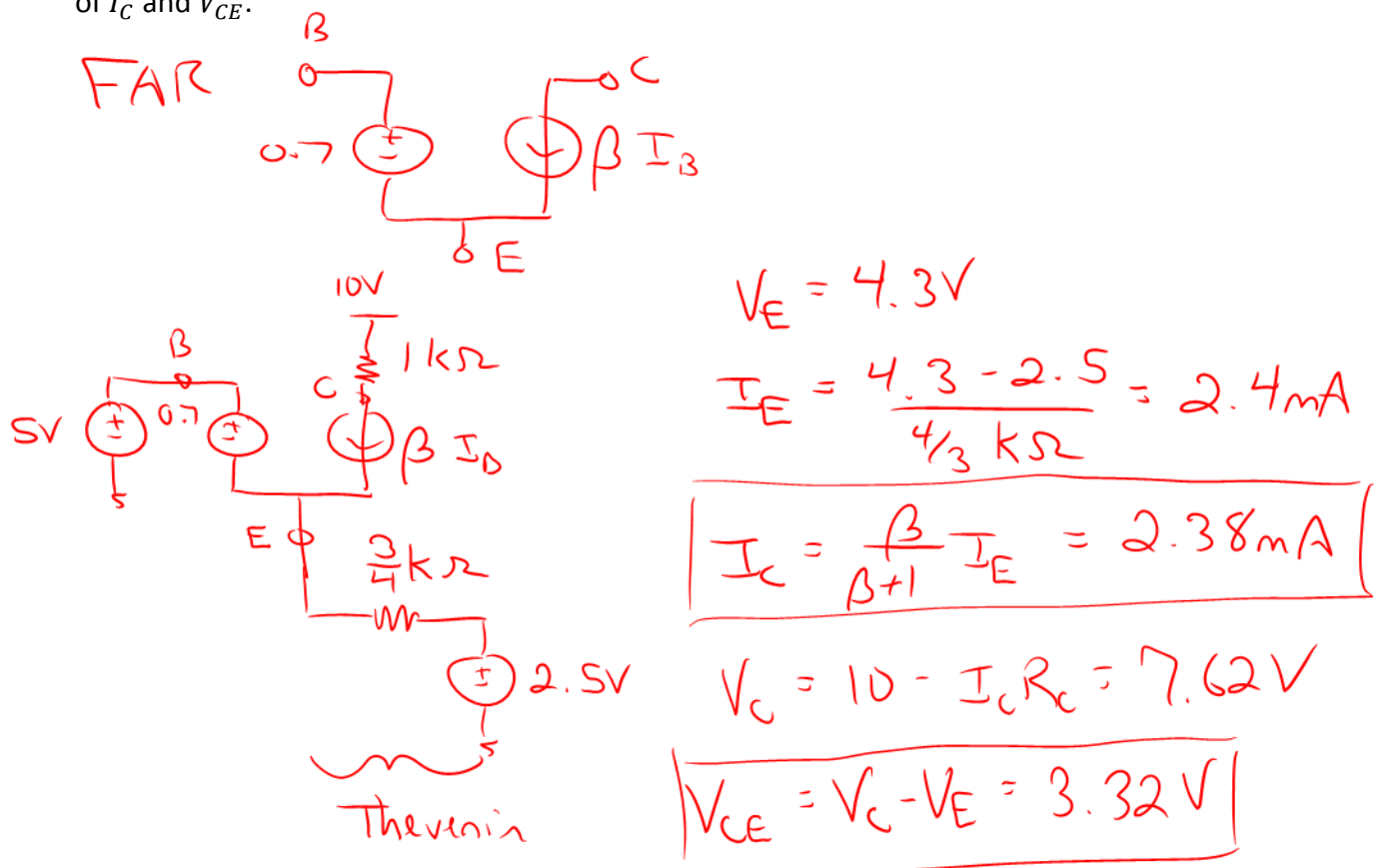
$$|V_{DS}| < |V_{GS}| - |V_{TP}| \Rightarrow \boxed{\text{LINEAR}}$$

**Problem 2 (20 Points):**

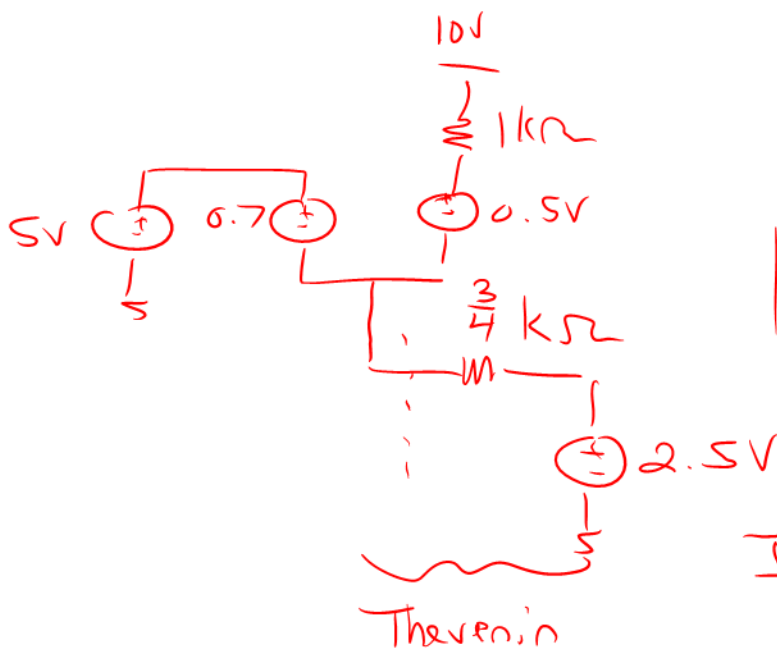
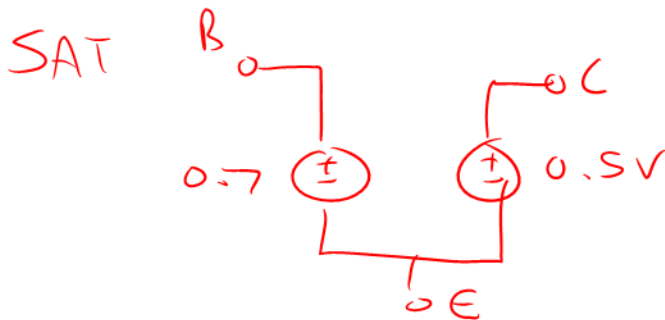
Use the following circuit and ignore base-width modulation for all parts.



- a) Substitute the simplified large-signal model for the BJT in the forward-active region using the constant-voltage source model for the base-emitter junction diode. Solve for the values of  $I_C$  and  $V_{CE}$ .



- b) Substitute the simplified large-signal model for the BJT in the saturation region using the constant-voltage source models for the base-emitter and collector-emitter voltages. Solve for the values of  $I_B$  and  $I_C$ .



$$V_E = 4.3V$$

$$V_C = 4.8V$$

$$I_C = \frac{10 - V_C}{1k\Omega} = 5.2mA$$

$$I_E = \frac{4.3 - 2.5}{\frac{3}{4}k\Omega} = 2.4mA$$

$$I_B = I_E - I_C = -2.8mA$$

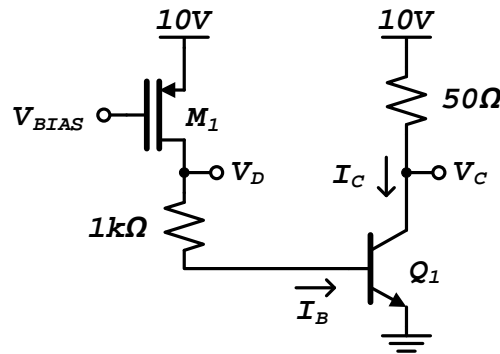
c) Given your answers to parts a) and b), is  $Q_1$  in the forward-active or saturation region.

For SAT assumption,  $I_B < 0$  which cannot happen for NPN

Forward Active Region



**Problem 3 (30 Points):** Use the circuit shown below to answer all of the following parts. Use the constant-voltage source model for the base-emitter junction diode of  $Q_1$ . Ignore channel-length modulation, body effect, and base-width modulation for all parts.



$$\mu_p C_{ox} \frac{W}{L} = 500 \mu A/V^2$$

$$V_{tp} = -1.0 V$$

$$V_{be(on)} = 0.7 V$$

$$V_{ce(sat)} = 0.5 V$$

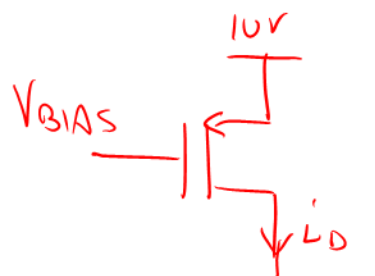
$$\beta_F = 100$$

- a) Assuming  $Q_1$  is kept in the forward-active region, find the numerical value of  $I_B$  required to support  $I_C = 1 mA$ .

Assuming FAR  $I_C = \beta I_B$

$$I_B = 10 \mu A$$

- b) Assuming  $M_1$  is kept in saturation, find the numerical value of  $V_{BIAS}$  required to support  $I_B$  from part a).



$$I_B = I_D = \frac{1}{2} \mu_p C_{ox} \frac{W}{L} (V_{gs} - V_{TP})^2$$

$$V_{gs} - V_{TP} = \pm \sqrt{I_D / \left( \frac{1}{2} \mu_p C_{ox} \frac{W}{L} \right)} = \pm 0.2V$$

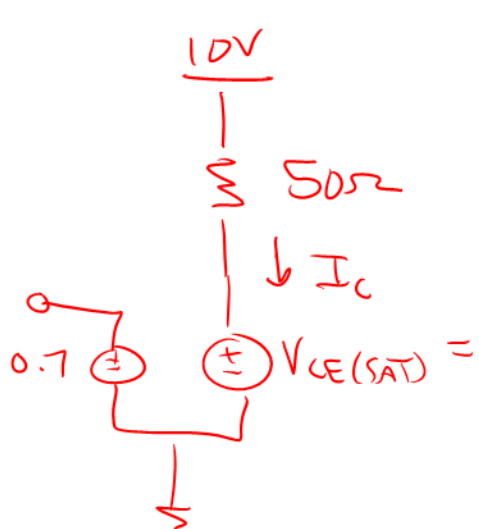
$$V_{gs} = V_{BIAS} - 10V$$

$$|V_{gs}| > |V_{TP}| \text{ for FET ON}$$

$V_{BIAS} = 8.8V$

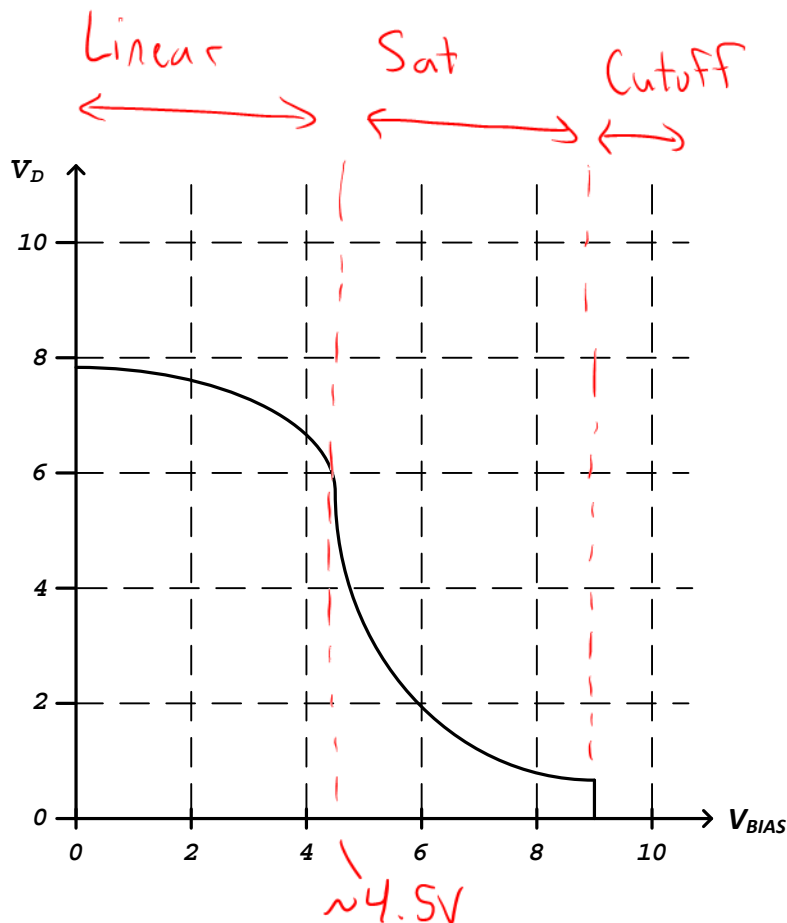
$$V_{gs} = -1.2V \Rightarrow |V_{gs}| - |V_{TP}| = 0.2V \text{ ON}$$

- c) Find the maximum value of  $I_C$  allowed while keeping  $Q_1$  in the forward-active region.

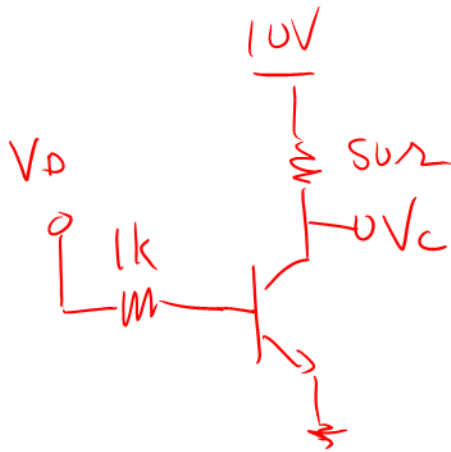


$$I_C = \frac{10 - 0.5}{50\Omega} = 190mA$$

- d) As  $V_{BIAS}$  is swept from 0 to 10 V, the drain voltage  $V_D$  follows the graph shown below. Label the regions on the graphs where  $M_1$  is in *cutoff*, *linear*, and *saturation*, specifically showing the values of  $V_{BIAS}$  at the boundaries between regions.



- e) Sketch the voltage at node  $V_C$  as  $V_{BIAS}$  is swept from 0 to 10 V. Use the graph from part d), giving you  $V_D$  as  $V_{BIAS}$  is swept over the same range, to generate your sketch. Label the regions on the graph where  $Q_1$  is in off, forward-active, and saturation.



$$\text{FAR: } V_C = 10 - \beta \frac{V_D - 0.7}{1k\Omega}$$

$$\text{SAT: } V_C = 0.5V$$

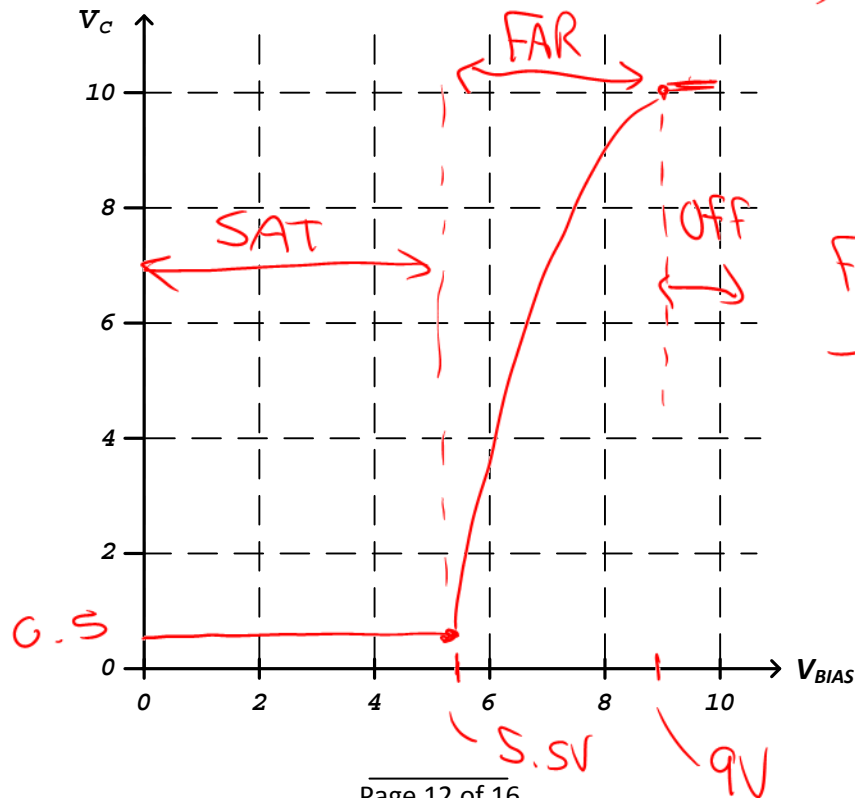
FAR/SAT Boundary:

$$I_C = 190\text{mA (from part c)}$$

$$I_B = 1.9\text{mA}$$

$$V_D = 0.7 + I_B \cdot 1k\Omega = 2.6V$$

From graph in d),  $V_{BIAS} = 5.5V$



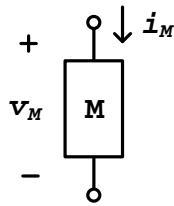
Results in  
 $V_D = 2.6$

FAR/SAT

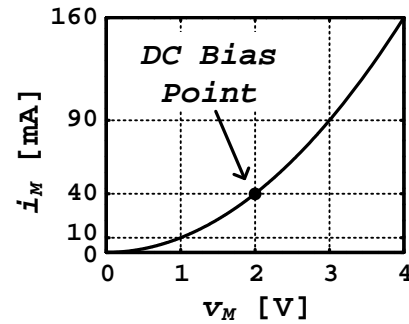
Transition at

$V_{BIAS} = 5.5V$

**Problem 4 (24 Points):** A non-linear two-terminal device  $M$  has the following I-V relationship, given in an expression and also plotted. Use this device to answer the following questions about small-signal analysis.



$$i_M = 0.01 \cdot v_M^2 \text{ A}$$



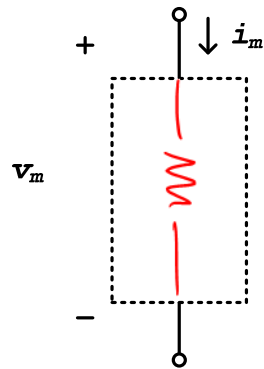
- a) Derive an expression for the small-signal conductance  $i_m/v_m$ , linearized around a DC operating point defined by variables  $I_M$  and  $V_M$ .

$$g_m = \left. \frac{\partial i_M}{\partial v_M} \right|_{DC \text{ op}} = 0.02 v_M \Big|_{V_M}$$

$$\boxed{g_m = 0.02 V_M}$$

- b) Complete the small-signal model by drawing the circuit element in the box that should be used to model the device in small-signal. Evaluate the value of this element at the bias current of  $I_M = 40 \text{ mA}$  as shown in the graph above.

**Small-Signal Model**



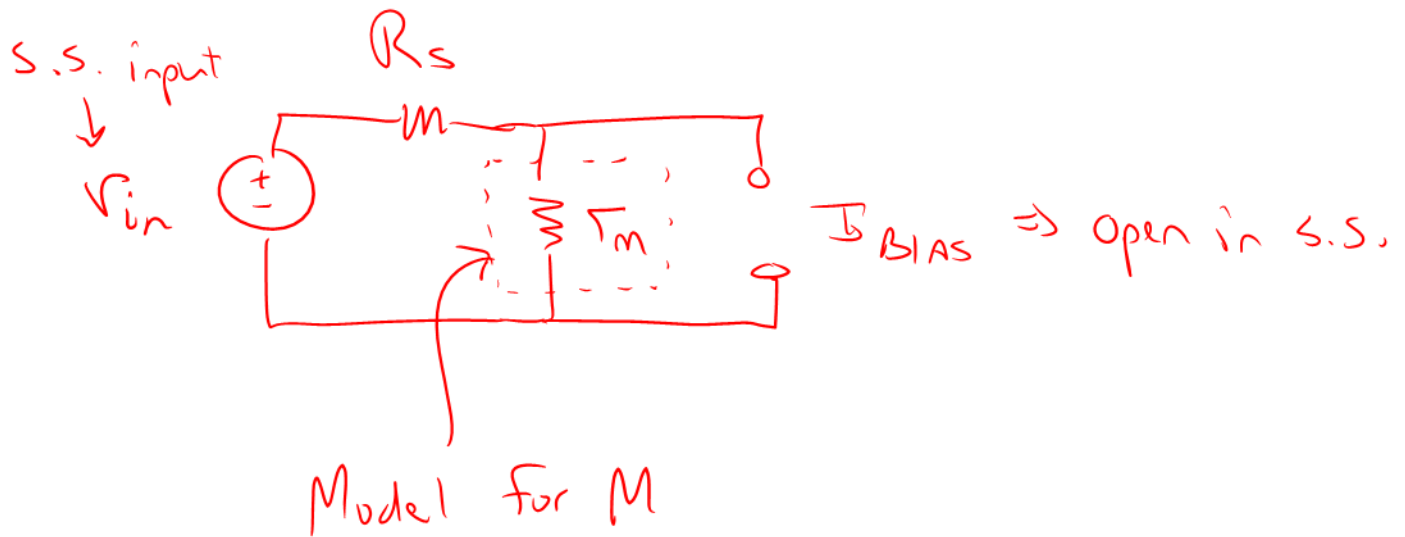
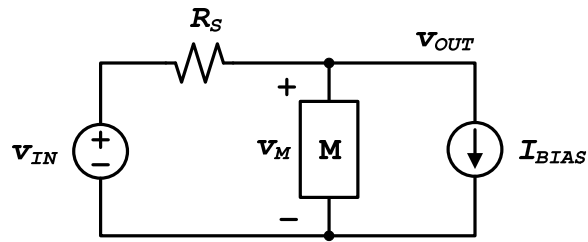
$$r_m = \frac{1}{g_m} = \frac{1}{0.02 V_M}$$

$$\text{At } I_M = 40 \text{ mA}, \quad V_M = 2 \text{ V}$$

$$r_m = \frac{1}{0.02 \cdot 2} = \boxed{25 \Omega}$$

Initials: \_\_\_\_\_

- c) The device is used in the following circuit. Draw the complete small-signal circuit, substituting the model for the device found in part b). Assume  $I_{BIAS}$  is a DC bias current.



(Space for additional work)