

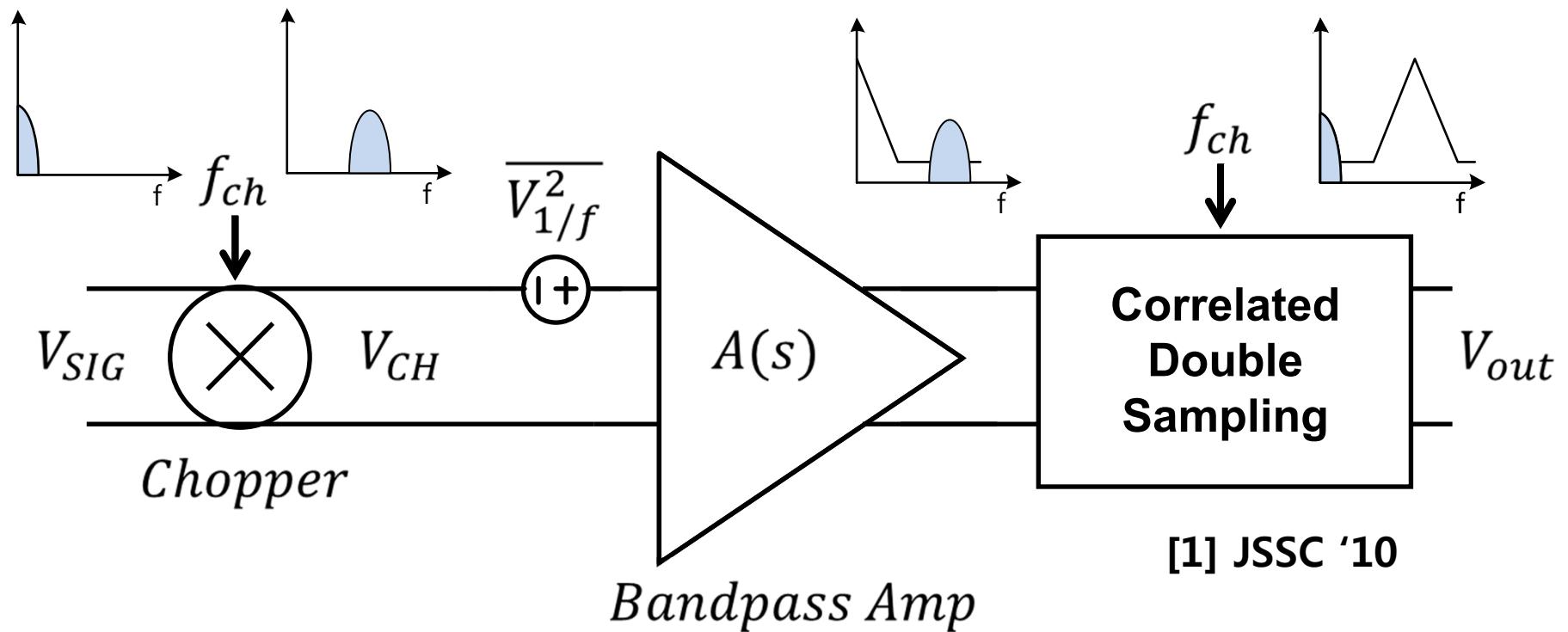
# Chopper–CDS Amplifier

Group 3

Jihyun Cho, Jaeyoung Kim and Inhee Lee

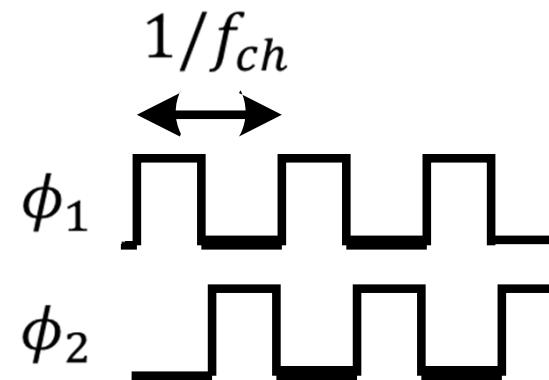
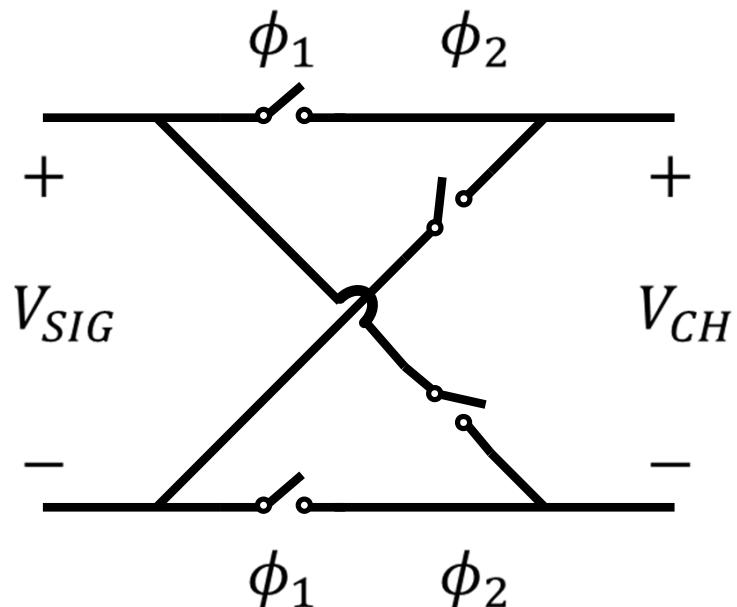
# Chopper Amplifier

- Input signal is at near DC (e.g. EEG)
- Up-convert before amp. to avoid 1/f noise



# Chopper

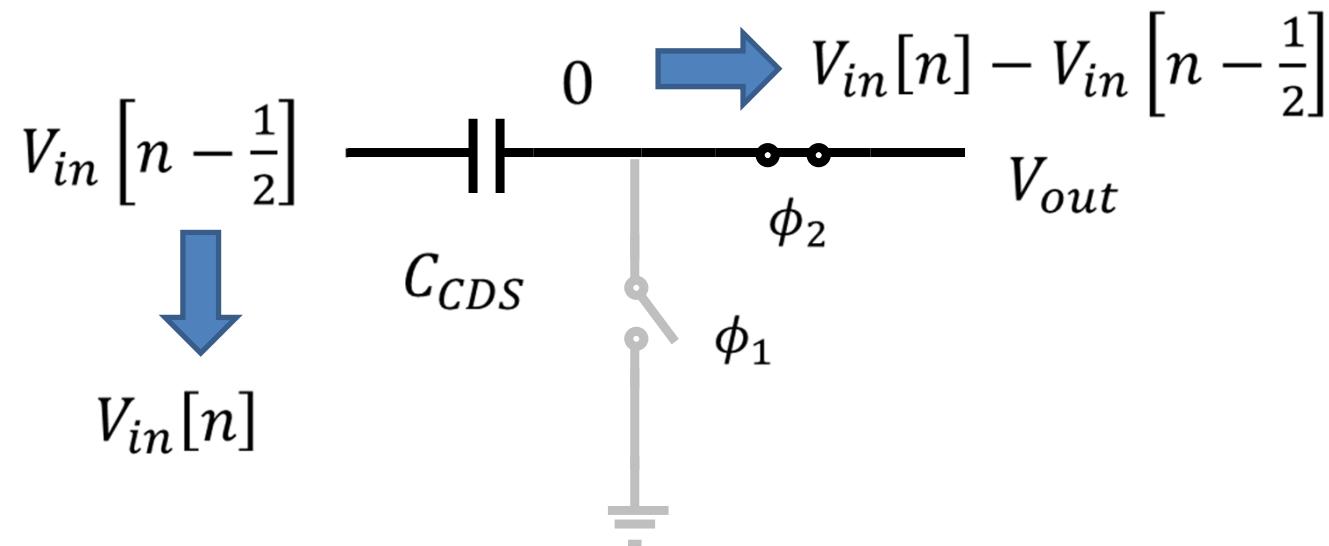
- Similar to commutating mixer



$$V_{CH} = \text{sign}(\phi_1) V_{SIG}$$

# Correlated Double Sampling

- Down-conversion by sampling
- Add a zero at DC



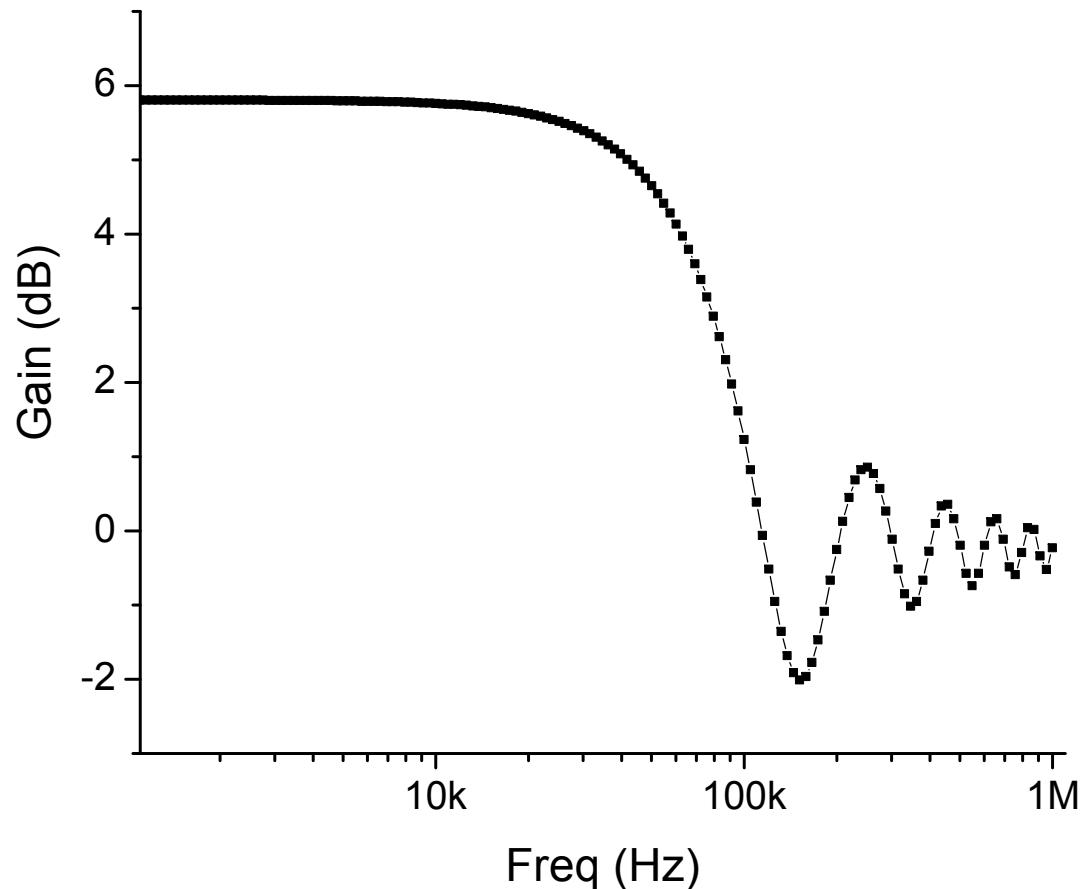
$$V_{out} = V_{in} \left[ 1 - z^{-\frac{1}{2}} \right]$$

# Chopper + CDS operation

- $V_{in} = \text{sign}(\phi_1) V_{SIG} + V_{os} + V_n$
- $V_{out} \sim \underbrace{(1 - z^{-1/2})V_{os}}_0 + \underbrace{(1 - z^{-1/2})V_n}_{\text{HPF}} + \underbrace{(1 + z^{-1/2})V_{SIG}}_2$ 
  - DC offset  $V_{os}$  is cancelled
  - Noise  $V_n$  is filtered (suppress 1/f)
  - Signal doubles (6 dB gain)  
(since signal changes sign every half cycle)

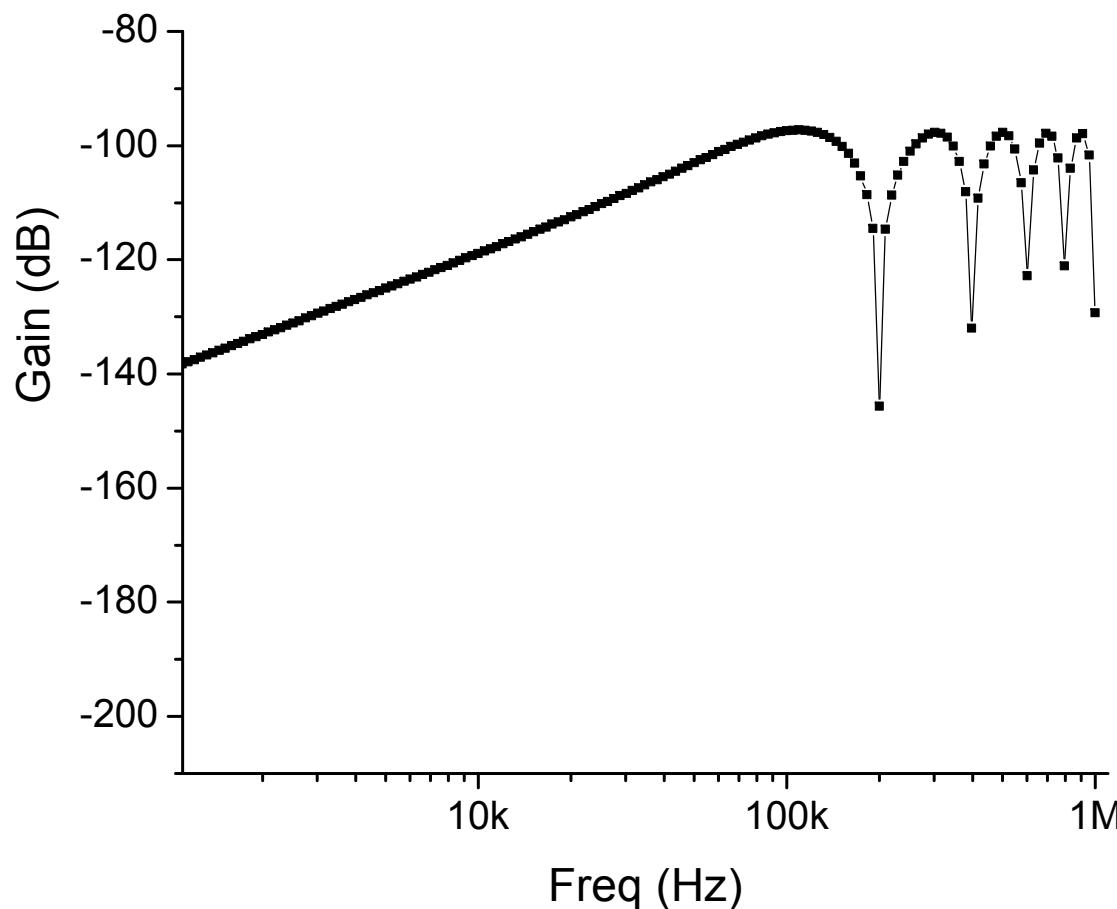
# Signal Transfer function

- +6dB signal gain at low frequency

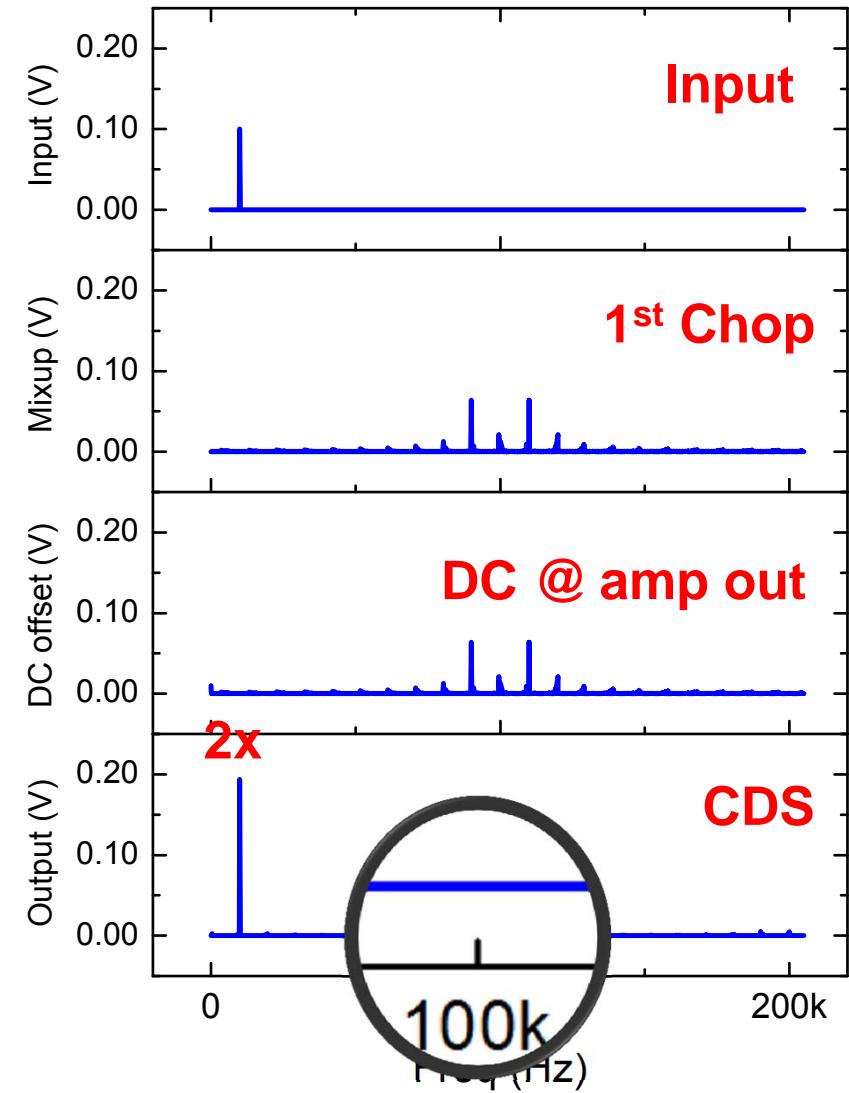
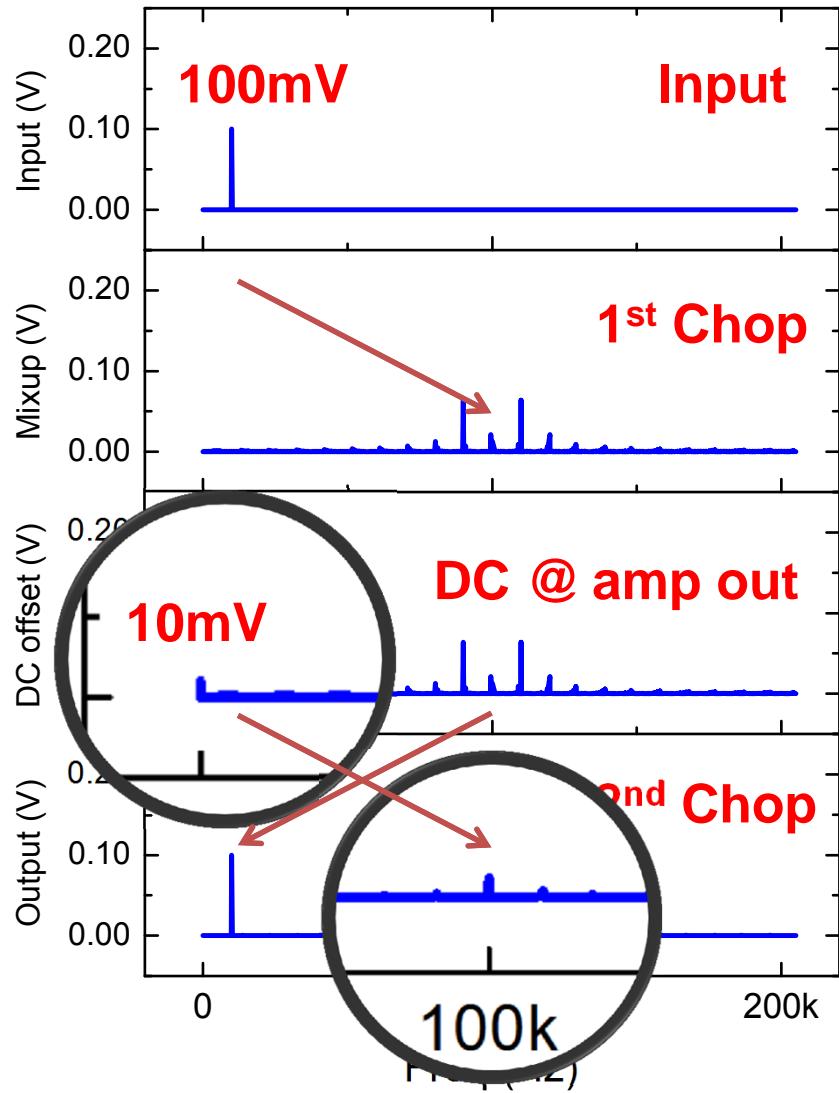


# Noise Transfer Function

- Filter out noise and DC at amp output

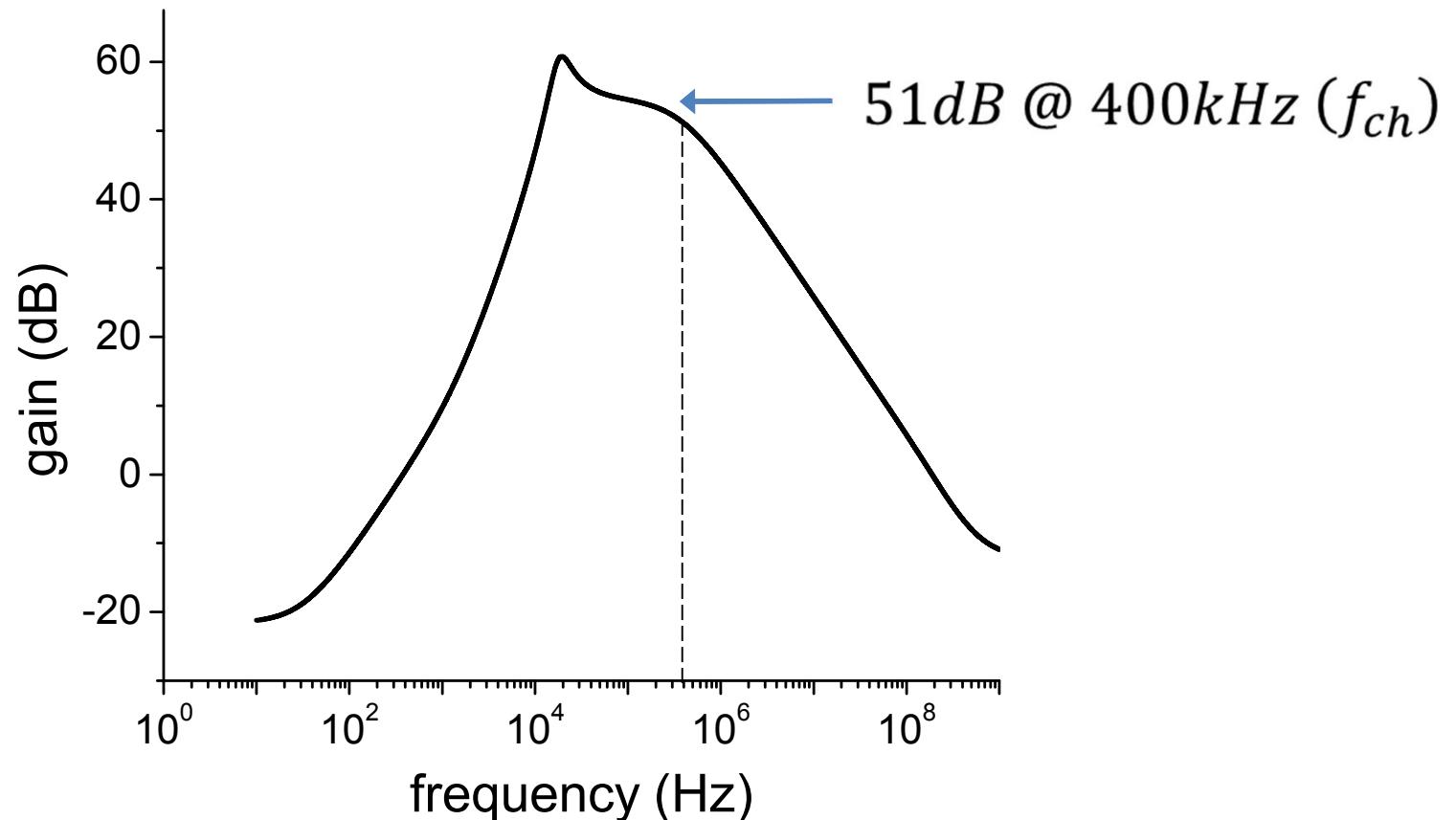


# Chopper vs. CDS

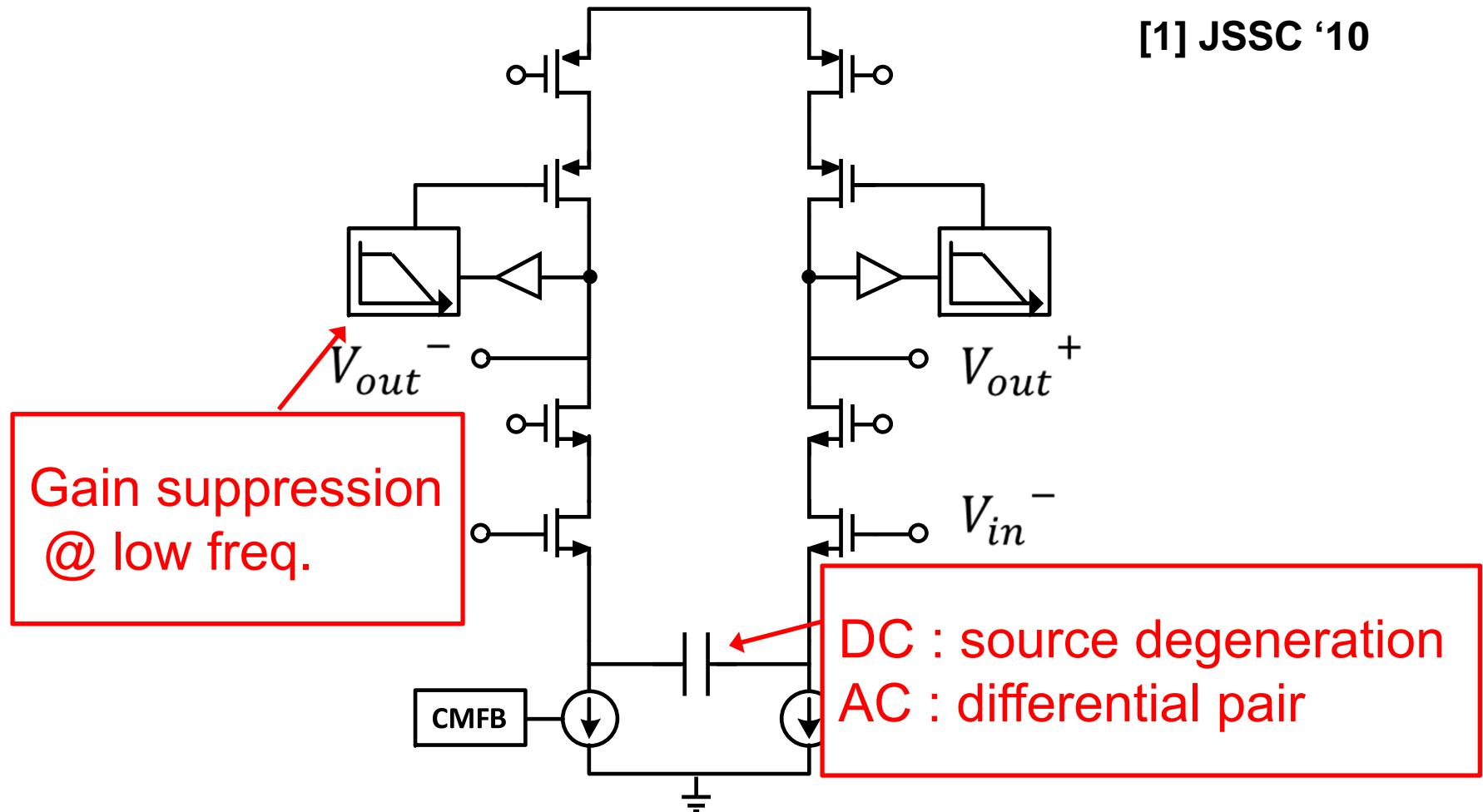


# Amplifier Design

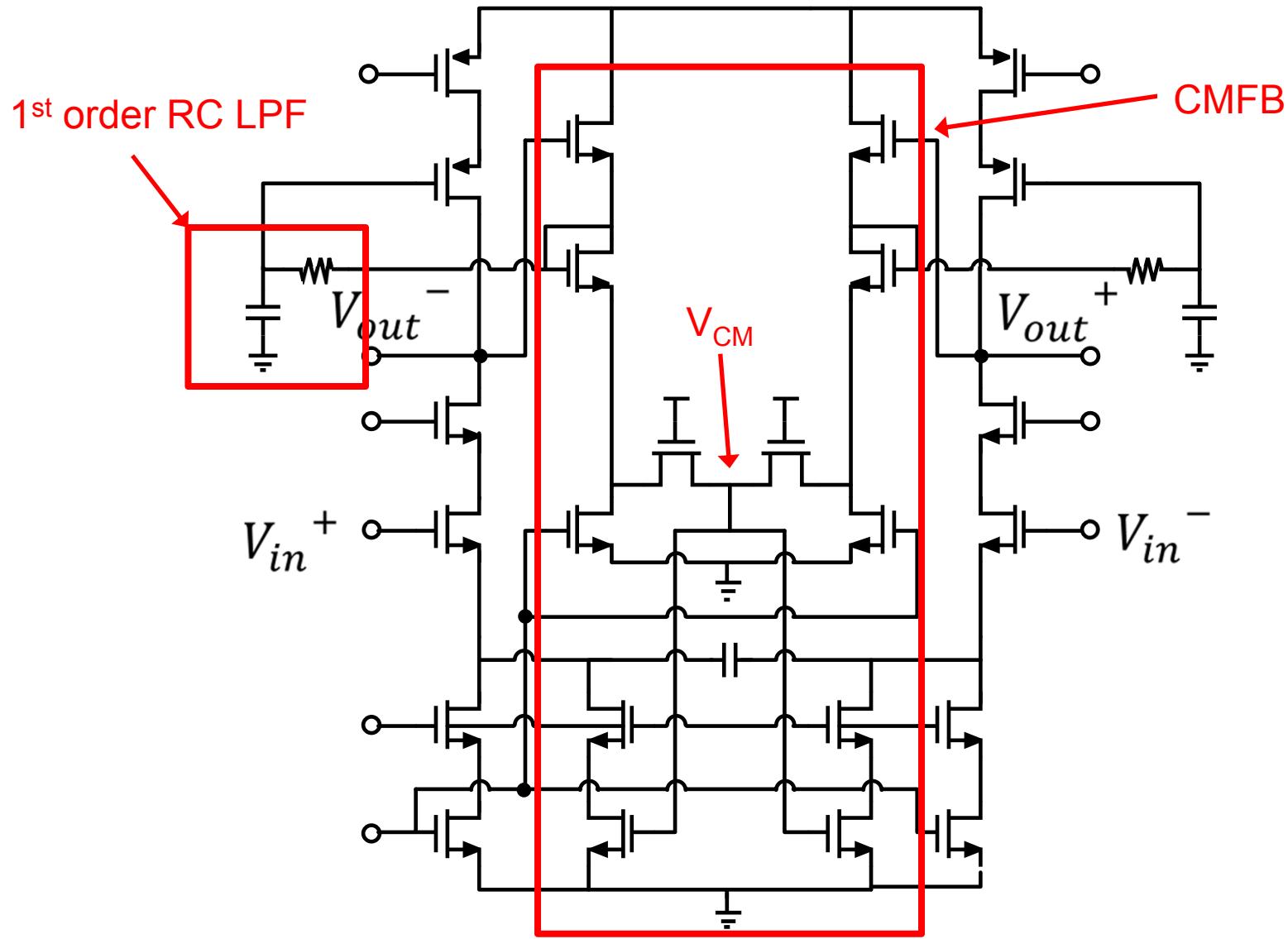
- Large offset → output saturation
- Bandpass response is required



# Bandpass Telescopic Amp.



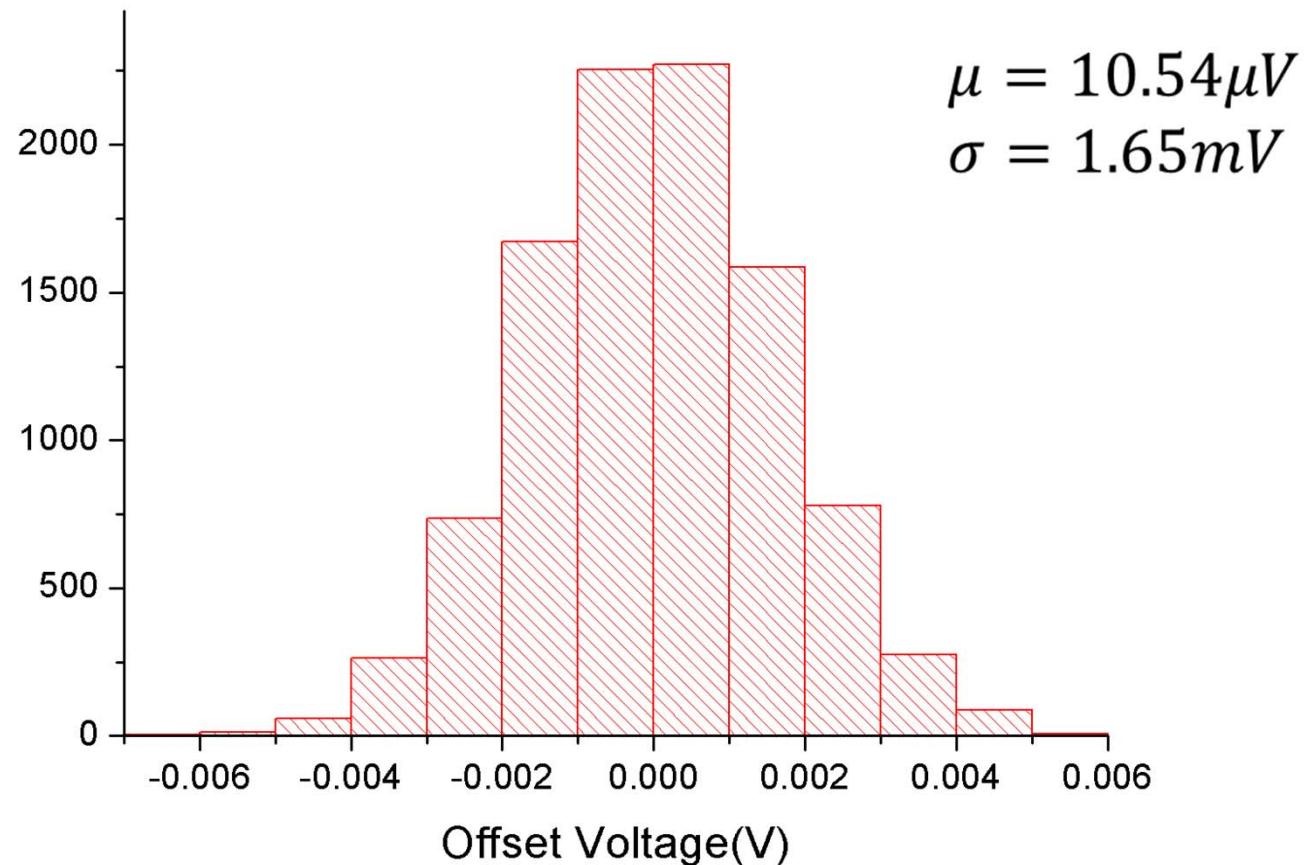
# Circuit Implementation



# Input Offset w/o BPF

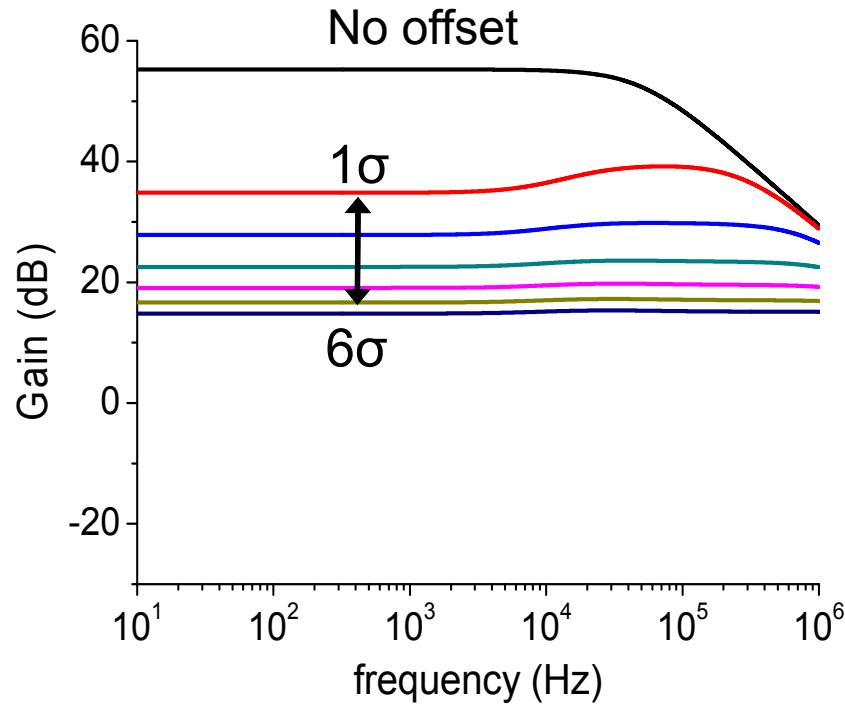
- Monte Carlo

# of iteration : 10K

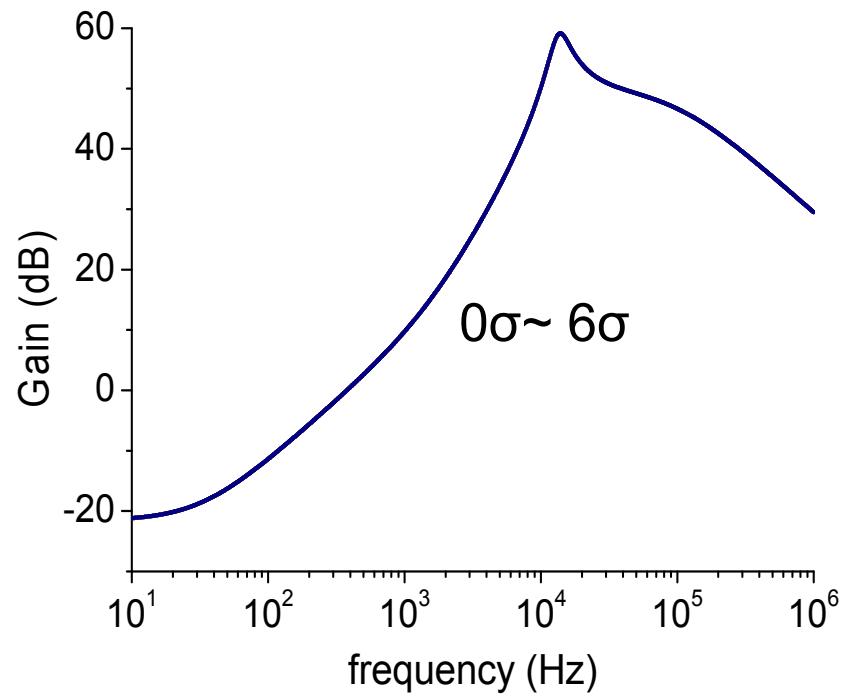


# AC Simulation w/ Offset

**Conventional Amp.**

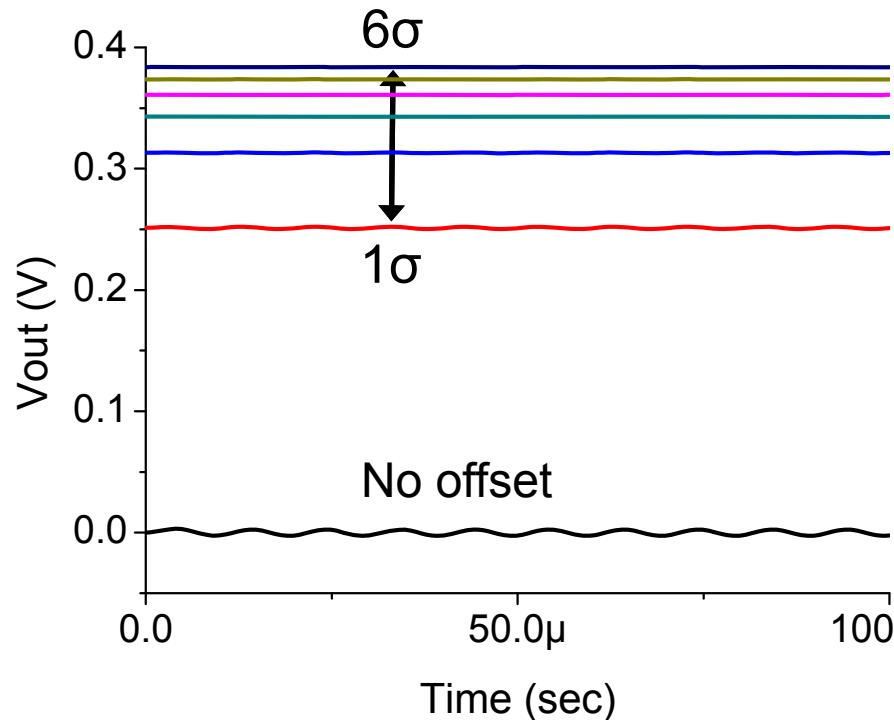


**This work (BP Amp.)**

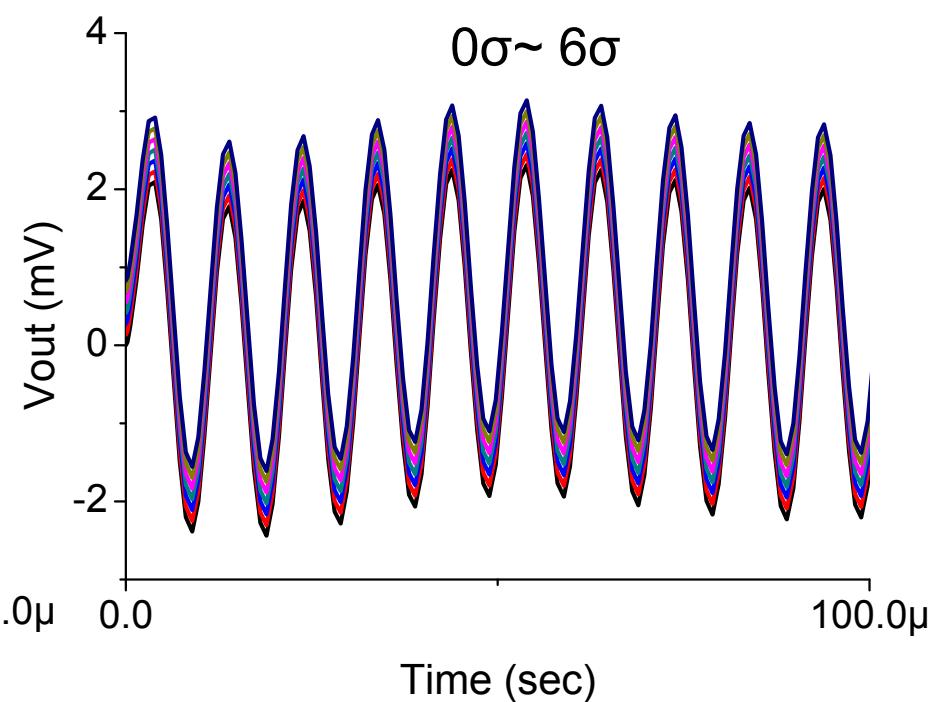


# Tran. Simulation w/ Offset

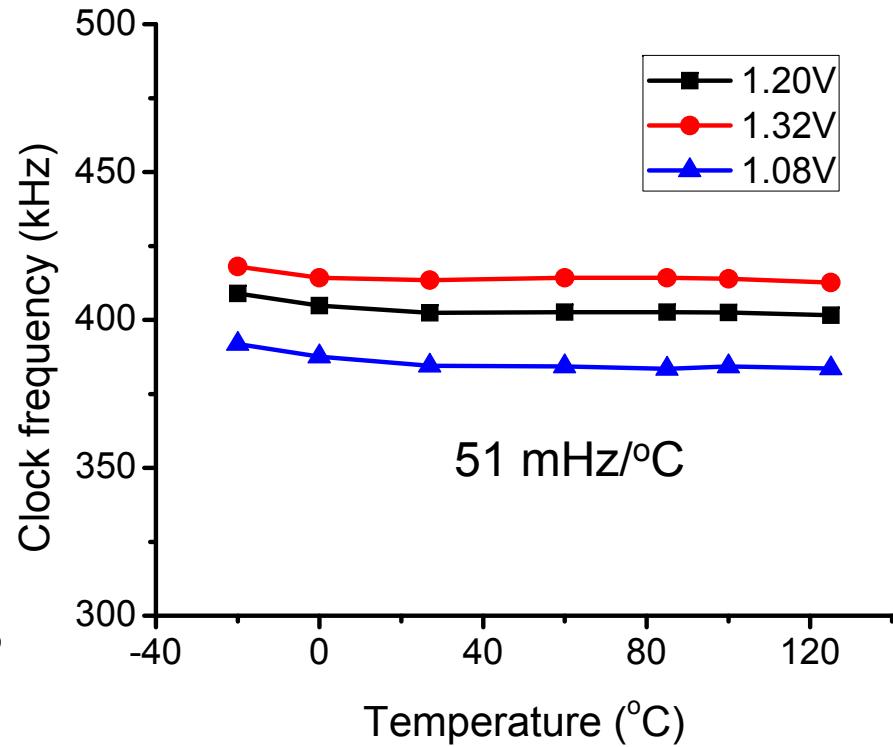
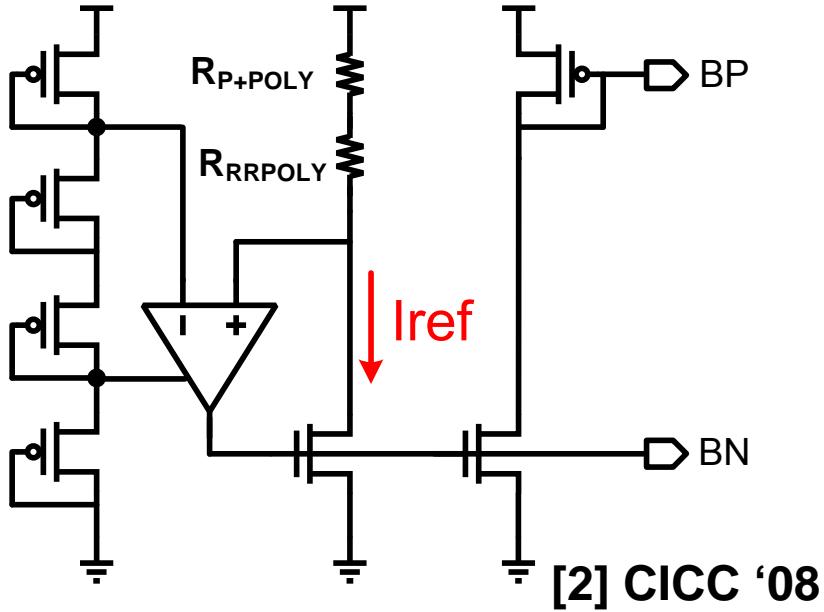
Conventional Amp.



This work (BP Amp.)

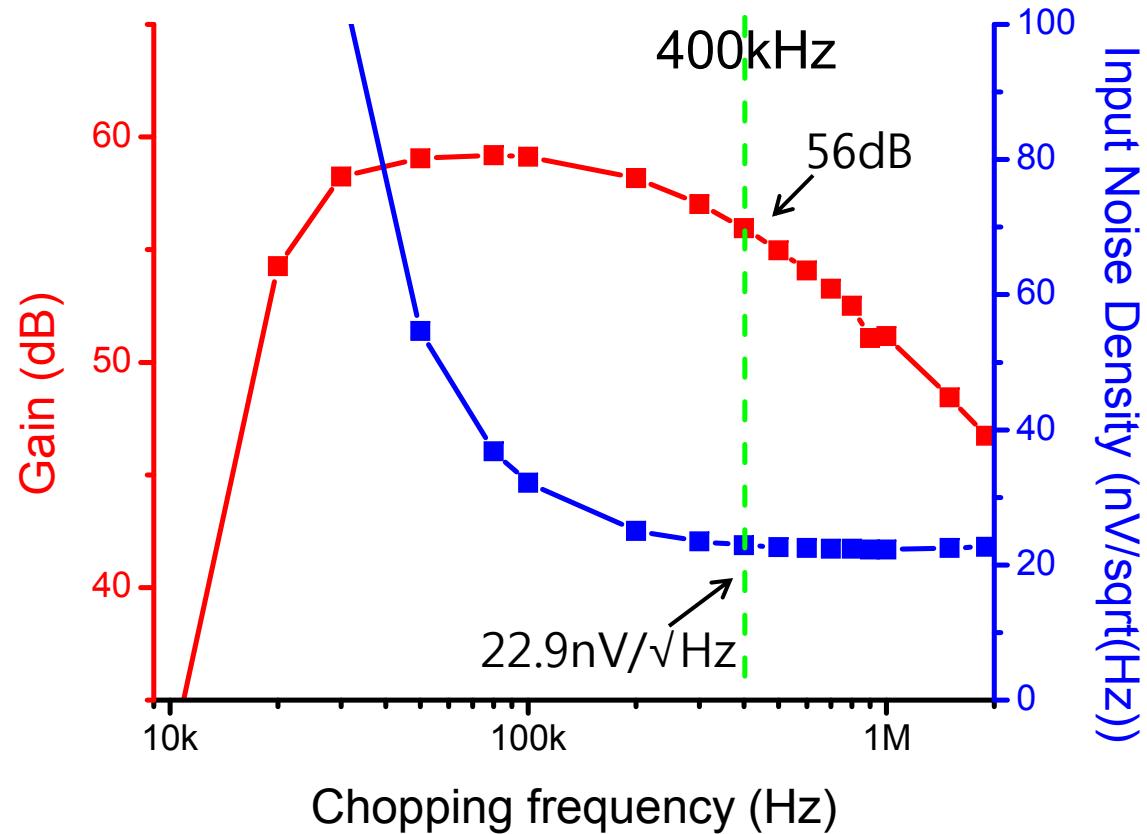


# Chopping Clock Generator



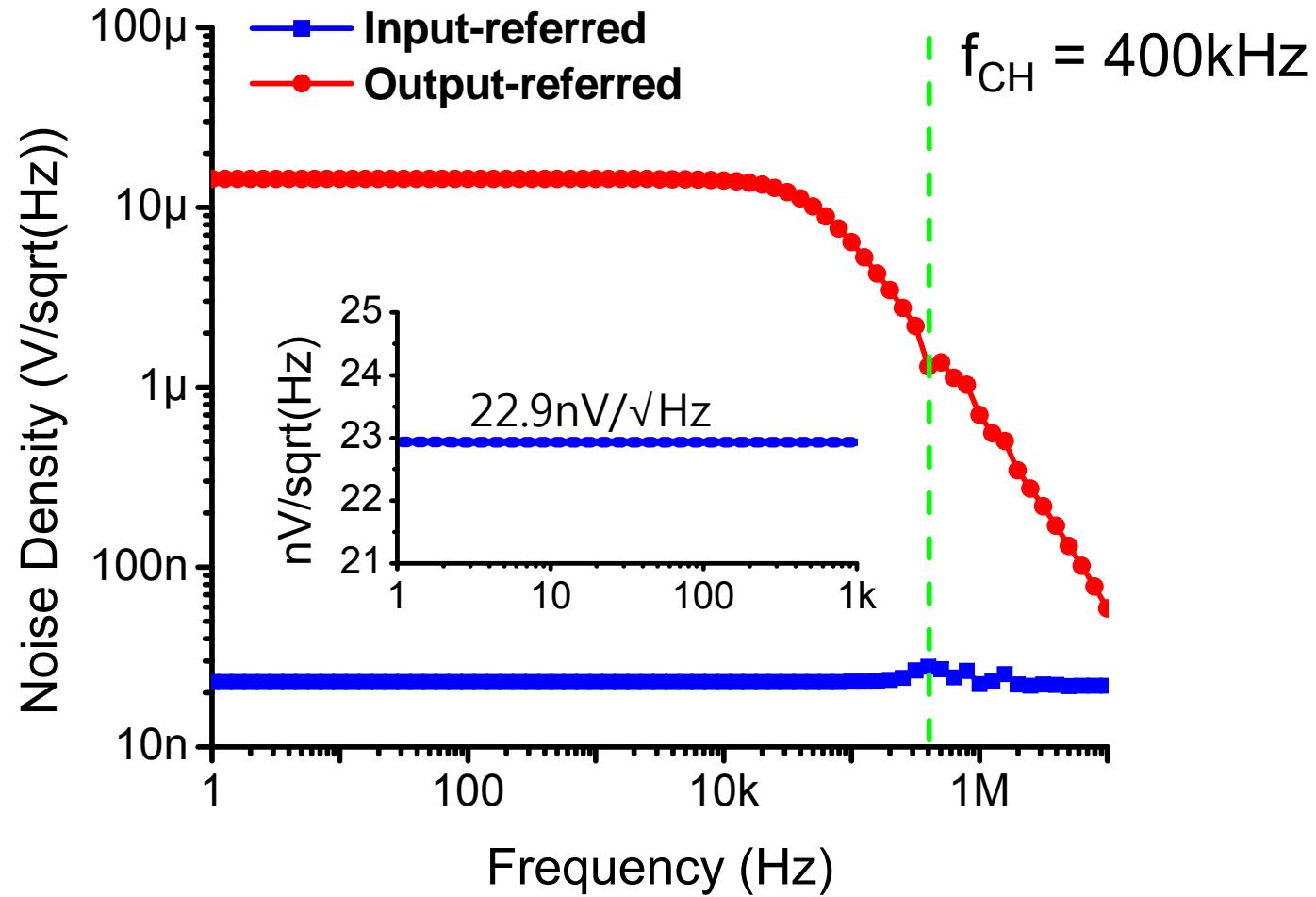
- Constant current reference
- Current starved inverter ring oscillator
- Temperature-insensitive clock

# Optimal Chopping Freq.



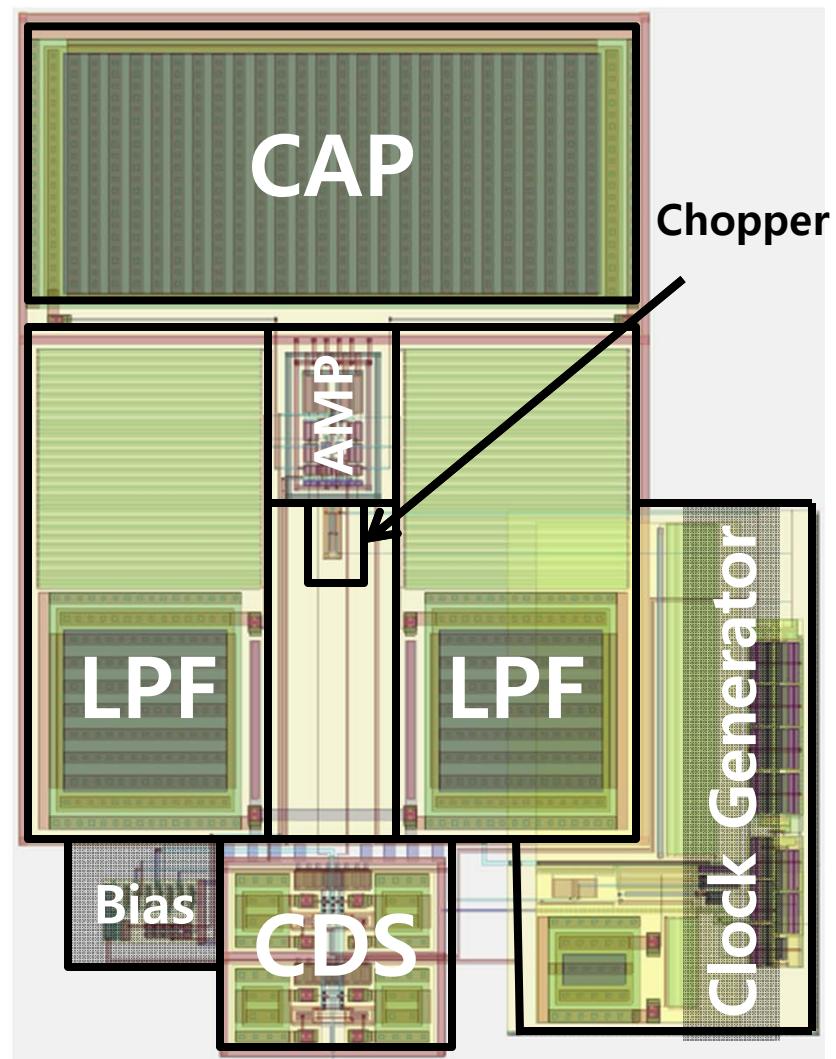
- Gain > Max – 3dB →  $f_{CH} = 400\text{kHz}$
- Min. input-referred noise density =  $22.3\text{nV}/\sqrt{\text{Hz}}$

# PNOISE Simulation



# Chip Layout

- Circuit blocks
  - Bandpass Amp.
  - Clock generator
  - Chopper
  - CDS
- Area :  $228\mu m \times 288\mu m$
- Symmetric Signal Path



# Performance Summary

	This Work	JSSC '10 [1]	ISSCC '11 [3]	ISSCC '10 [4]	JSSC '10 [5]
<b>Process [μm]</b>	0.13	0.18	0.35	0.70	0.35
<b>V<sub>DD</sub> [V]</b>	1.2	1.8	5.0	5.0	1.8
<b>Input Noise [nV/√Hz]</b>	23	37	6	11	95
<b>I<sub>DD</sub> [μA]</b>	13.5 (*26.9)	14.4	1500	143	13
<b>FOM (V<sub>NI</sub><sup>2</sup> /Δf)* I</b>	7.1 (*14.1)	19.7	51.2	15.8	117
<b>f<sub>CH</sub> [kHz]</b>	400	500	200	30	50
<b>DC Gain [dB]</b>	56	168	150	100	130
<b>Area [mm<sup>2</sup>]</b>	0.06	1.14	1.26	1.8	0.64

\* Current consumption is doubled for only 1<sup>st</sup> stage design

# Reference

- [1] M. Belloni, E. Bonizzoni, A. Fornasari, and F. Maloberti, "A Micropower Chopper—CDS Operational Amplifier", *IEEE J. Solid-State Circuits*, vol. 45, no 12, pp. 2521-2529, Dec., 2010.
- [2] Y. Lin, D. Sylvester, and D. Blaauw, "An Ultra Low Power 1V, 200nW Temperature Sensor for Passive Wireless Application," *CICC*, pp. 507-510, Sept., 2008.
- [3] Y. Kusuda, "A 5.9nV/ $\sqrt{\text{Hz}}$  Chopper Operational Amplifier with 0.78 $\mu\text{V}$  Maximum Offset and 28.3nV/ $^{\circ}\text{C}$  Offset Drift," *ISSCC Dig. Tech. Papers*, pp. 242-243, Feb., 2011.
- [4] Q. Fan, J.H. Huijsing, and K.A.A. Makinwa, "A 21nV/ $\sqrt{\text{Hz}}$  Chopper-Stabilized Multipath Current-Feedback Instrumentation Amplifier with 2 $\mu\text{V}$  Offset," *ISSCC Dig. Tech. Papers*, pp. 80-81, Feb., 2010.
- [5] Y. Kusuda, "Auto Correction Feedback for Ripple Suppression in a Chopper Amplifier," *IEEE J. Solid-State Circuits*, vol. 45, no 8, pp. 1436-1445, Aug., 2010.