

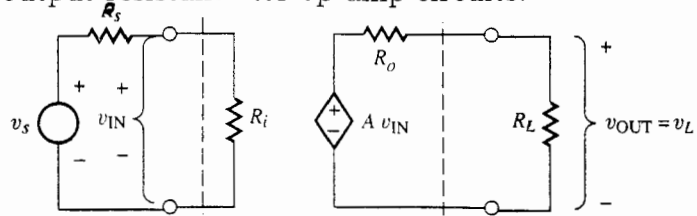
INPUT AND OUTPUT RESISTANCE FOR OP-AMP CIRCUITS *ay*

SIGNIFICANCE of input and output resistance for op-amp circuits:

Overall voltage gain $A' = \frac{v_{OUT}}{v_s}$

$$= A \frac{R_i}{R_i + R_s} \frac{R_L}{R_o + R_L} < A$$

$\rightarrow A$ as $R_i \rightarrow \infty$ and $R_o \rightarrow 0$.



DETERMINING input and output resistance for op-amp circuits:

INPUT: Connect a V_{test} to *input* and compute resulting I_{test} . $R'_i = \frac{V_{test}}{I_{test}}$.

OUTPUT: Connect a V_{test} to *output* and compute resulting I_{test} . $R'_o = \frac{V_{test}}{I_{test}}$.

For output impedance R'_o , set *input* voltage $v_s = 0$ and omit load R_L .

Note this is just the Thevenin resistance of the amplifier output.

GAIN: Connect a V_{test} to *input* and compute v_{OUT} . $A' = \frac{v_{OUT}}{v_s}$. Omit load R_L .

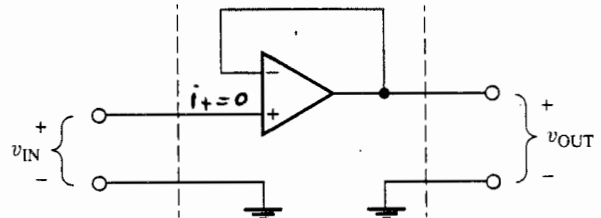
EXAMPLES of input and output resistance for op-amp circuits:

THE IDEAL $R'_i = \frac{V_{test}}{I_{test}} = \frac{V_{test}}{i_+} \rightarrow \infty$

FOLLOWER $R'_o = \frac{V_{test}}{I_{test}} |_{v_{IN}=0} = \frac{0}{I_{test}} = 0$

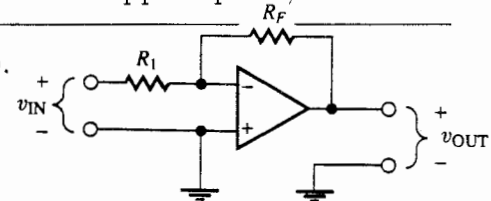
(since $v_{out} = 0$ we can't connect a $V_{test} \neq 0$ without producing an explosion!)

A follower is an ideal "front end": it draws no current and supplies plenty.



INVERTING $R'_i = \frac{V_{test}}{I_{test}} = R_i$ (obvious since $v_- = 0$).

AMPLIFIER $R'_o = \frac{V_{test}}{I_{test}} |_{v_{IN}=0} = \frac{0}{I_{test}} = 0$



NON-IDEAL $R'_i = \frac{V_{test}}{I_{test}} = R_i \frac{(A+1)R_L + R_o}{R_L + R_o} + \frac{R_o R_L}{R_o + R_L}$

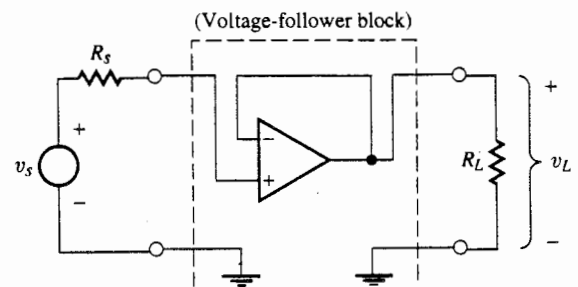
FOLLOWER $R'_o = \frac{V_{test}}{I_{test}} = \frac{R_o(R_i + R_s)}{R_o + (A+1)R_i + R_s}$

$$A' = \frac{v_{OUT}}{v_s} = \frac{R_o + AR_i}{R_o + (A+1)R_i}$$

SIGNIFICANCE: Using typical op-amp values

$A = 10^5$, $R_i = 2M\Omega$, $R_o = 75\Omega$, and a load $R_L = 1\Omega$ and source resistance $R_s = 1M\Omega$, the follower *still* acts almost ideally.

But other circuits (see p.161) may not!



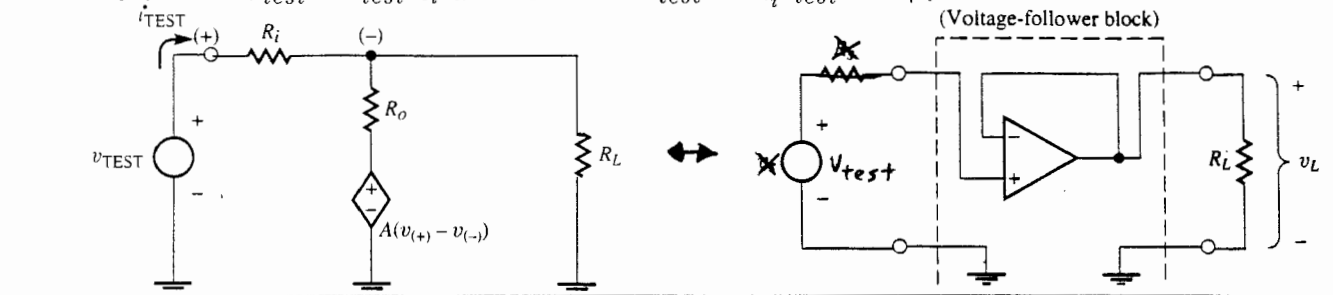
Let $R_i \rightarrow \infty$, $R_o \rightarrow 0$, $A \rightarrow \infty$. Then non-ideal results \rightarrow ideal results.

DETAILS OF ANALYSIS (also see Schwarz and Oldham p. 154-6):

INPUT: In figure below, write node equation at $v_- = v_{out}$ and note $v_+ = V_{test}$:

$$\frac{v_- - V_{test}}{R_i} + \frac{v_- - A(V_{test} - v_-)}{R_o} + \frac{v_-}{R_L} = 0$$

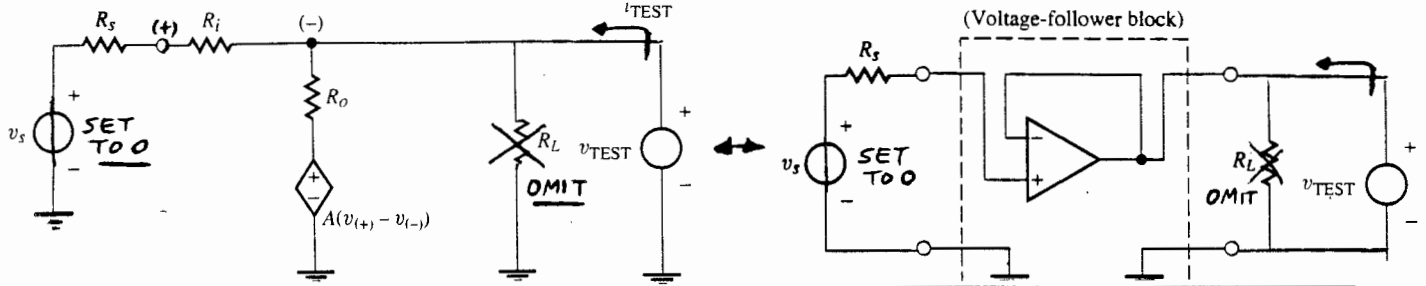
Insert $v_- = V_{test} - I_{test}R_i$ and solve for $V_{test} = R'_i I_{test} \rightarrow R'_i$.



OUTPUT: See figure below. We have (note voltage divider)

$$I_{test} = \frac{V_{test}}{R_i + R_s} + \frac{V_{test} - A(-V_{test} \frac{R_i}{R_i + R_s})}{R_o} = V_{test} \frac{R_o + R_i + R_s + AR_i}{R_o(R_i + R_s)}$$

from which we get $R'_o = \frac{V_{test}}{I_{test}} = \frac{R_o(R_i + R_s)}{R_o + (A+1)R_i + R_s}$.



GAIN: See figure at right. We have

$$i_1 = \frac{V_{test} - A(V_{test} - v_{out})}{R_o + R_i}$$

and $v_{out} = V_{test} - i_1 R_i$. Substituting gives

$$A' = \frac{v_{OUT}}{v_{test}} = \frac{R_o + AR_i}{R_o + (A+1)R_i}$$

